# PREDICTING SOIL LOSS

# USING THE UNIVERSAL SOIL LOSS EQUATION





**ARKANSAS** 

U.S. DEPARTMENT OF AGRICULTURE, SOIL CONSERVATION SERVICE, LITTLE ROCK, ARKANSAS

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#### INTRODUCTION

This handbook contains guidelines for selecting erosion control practices best suited to the particular needs of Arkansas soils, whether intended for agricultural or non-agricultural use.

It outlines a procedure for predicting soil loss from sheet erosion through the use of the Universal Soil Loss Equation. This technique utilizes all pertinent research information which has been methodically combined to provide design data for conservation plans. It is not intended for use in predicting gully erosion caused by concentrated flowing water, or for wind or geologic erosion.

Accurate predictions of soil loss can be made for croplands, grasslands, woodlands and urban developments. This technique gives planners a means for precisely evaluating the effectiveness of various conservation treatments and a basis for making sound choices from the acceptable alternatives.

The Universal Soil Loss Equation is the result of more than 20 years of study and development by scientists of the USDA. Science Education Administration Research is continuing to obtain still more precise information on the interrelations of topography, soil, and management practices. As additional knowledge is gained, it will be incorporated into the present prediction procedure.

#### THE EQUATION

The Universal Soil Loss Equation (USLE) is expressed: A=RKLSCP, wherein:

- A is the predicted soil loss;
- R is the rainfall factor
- K is the soil-erodibility factor;
- L is the slope-length factor;
- S is the slope-gradient factor;
- C is the cropping-management factor; and
- P is the erosion-control practice factor.

Numerical values for each of the six factors have been determined from research data. These values differ from one field or locality to another and may be determined from the figures and tables presented herein.

Predicted soil loss is the calculated annual soil loss expressed in tons per acre. Sheet erosion is sometimes difficult to detect because five tons of soil removed evenly from one acre amounts to a layer of only 0.0275 inches, or less than the thickness of a dime. See Table 1 for time required to erode one inch of soil per acre. To convert to cubic yards, see Table 7.

Table 1
Years Required to Erode 1 Inch of Soil Per Acre

		of Soil re-inch)	3	Soil	Loss 5	Rate 6	(tons	per 8	acre	per 10	year) 11	12
	136	)	44	34	27	23	19	17	15	14	12	11
	142	-Clays	47	36	28	24	20	18	16	14	13	12
Loams-	147		49	37	29	24	21	18	16	15	13	12
	152		51	38	30	25	55	19	17	15	14	13
	158		53	40	32	26	23	20	18	16	14	13
j	165		55	41	33	28	24	21	18	16	15	14
	171	-Sands	57	43	34	28	24	21	19	17	16	14
	176	)	59	44	35	29	25	22	20	18	16	15
	182		61	46	36	30	26	23	20	1.8	17	15

#### "R" FACTORS and "EI" VALUES

R is the rainfall erosion factor. An R value indicates the erosivity of the rainfall, not the average annual precipitation in a locality. Fig. 1 shows the distribution of R values in Arkansas by counties.

R values are adjusted to estimate soil losses during years when storms are above average and to estimate losses from individual storms. Table 6 lists probability values for 5, 20, and 50 percent probabilities and expected magnitudes of single storm EI values for 1, 2, 5, 10, and 20 years.

An R value is defined as the number of erosion index (EI) values in a normal year's rain. The erosion index (EI) value of a given storm is equal to the kinetic energy of the storm in hundredths of foot-tons per acre times its maximum 30-minute intensity in inches per hour. The EI values of individual storms may be summed to get an EI value for a month, for six months, or for any period of time. When EI values are summed and averaged over a period of years they become R values.

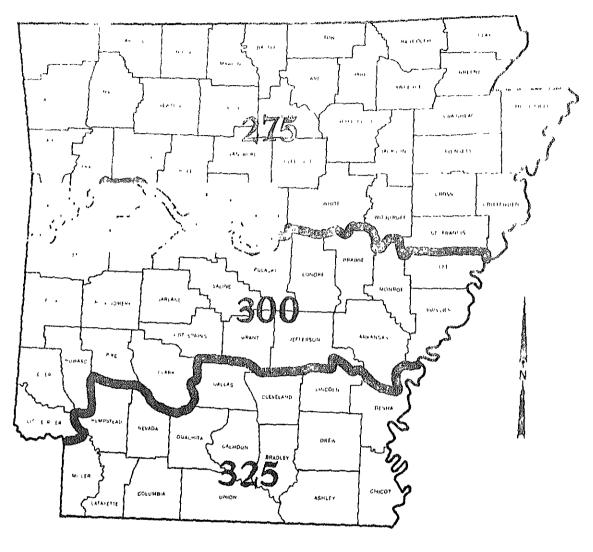
EI values, like R values, vary from one locality to another. There are three EI values in Arkansas as shown in Figure 2.

The distribution of erosive rains (or EI values) becomes important when C values, or estimates of soil losses, for a period of less than one year are needed. The distribution may be presented as a curve on a graph or in tabular form. Both methods show distribution as percent of EI at 10 day intervals. EI values used in Arkansas are included in Table 2.

Example - Determine the EI value (erosive rains) for the period April 1 to April 20 at Little Rock, Arkansas.

First: Refer to Figure 2 and note that erosion-index distribution No. 22 is applicable to Little Rock.

Second: See Table 2 - Under Curve No. 22 the reading for April 1 is 22 and the reading for April 20 is 30. The difference between these two readings -8- represents the percent of the average annual erosive rains that can be expected to occur during this period.



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# FIGURE 1 AVERAGE ANNUAL VALUES OF RAINFALL FACTORS

#### "K" FACTORS

K is the soil-erodibility factor. It is defined as the rate of crosion per unit of erosion index from unit plots on a given soil. A unit plot is one 72.6 feetlong and has a uniform lengthwise slope of name percent. Unit plots are kept in continuous fallow and free of vegetation for at least two years or until all crop residues have decomposed before they are used to determine K factors. When measurements are to be made, the plots are plowed in the spring and prepared for planting crops by conventional methods. Additional tillage is used as needed to control vegetation and prevent crusting. All tillage operations are performed up and down the slope. Naturally, soil losses from plots subjected to such treatments are among the highest that we could expect. These losses, soil by soil, are the basis for determining K factors. Soil losses from unit plots are also the basis for the soil-loss ratios used to compute C factors.

Unit plots have been established at several research centers across the country and K factors have been measured by research techniques for more than twenty major soils.

More than 25 characteristics of a soil affect its susceptibility to water erosion. These characteristics may be grouped into two major categories: those that influence infiltration, permeability and total water holding capacity; and those that affect dispersion, splashing, abrasion, and transportation of soil particles by runoff. The K factors originally assigned to most soils reflect the erodibility of the surface layer only. Due to increased interest in predicting soil losses from construction sites and similar areas, K factors have been determined for different layers of a soil. A soil series may now have as many as five K factors assigned to it depending on the characteristics of its profile.

Obviously, it is not practical to determine all K factors by research methods so the K factors for most soils are assigned after comparing them with similar soils that have measured factors. Assigned K factors are approved for each soil series by the regional principal soil correlator upon recommendations by soil scientists, agronomists, and other specialists. The assigned values are reviewed as new information becomes available and new lists of K factors are published from time to time. K factors and T factors for Arkansas soils are listed in Table 8. (See appendix.)

### "T" VALUES

"T" is the soil loss tolerance value. It indicates the rate of soil loss in tons per acre per year that will allow a high level of crop production to be sustained economically and indefinitely. Any combination of cropping and management practices which will keep soil losses at or below the specified T value for a soil will provide satisfactory erosion control for that soil. T values for croplands range from 1.0 to 5.0 tons per acre.

#### "L" and "C" FACTORS

L and S are the topographic factors in the equation. L is the length of slope factor. S is the steepness of the slope factor. L and S have independent effects on water erosion; however, in this equation they are considered together as the LS factor and their values indicated numerically as soil-loss ratios.

The factor LS is the expected ratio of soil loss per unit area on a field slope to corresponding loss from the basic 9-percent slope, 72.6 feet long.

Refer to Table 9 (see appendix) for LS factor values.

Slope length begins at the point where runoff begins. It ends where the slope decreases, deposition begins, or where runoff enters a well defined channel that may be part of a drainage network or a constructed channel such as a terrace or diversion.

#### "C" FACTORS

C is the cropping-management factor (cropland and other uses) in the equation. It is the ratio of soil loss from a field with specified cropping and management or plant cover, to that from the fallow condition on a unit plot 72.6 feet long, with a uniform lengthwise slope of 9 percent in continuous fallow, tilled up and down the slope. This factor measures the combined effect of all the interrelated cover and management variables plus the growth stage and vegetal cover at the time of the rain.

Refer to Table 10 for C values for cropland.

Refer to Table 11 for C values for pasture, range, and idle land.

Refer to Table 12 for C values for woodland.

Refer to Table 13 for C values for annual cover and various quantities of mulch cover or mulch.
"P" FACTORS

P is the erosion control practice factor. Erosion control practice in this case refers to contour farming and contour stripcropping or the lack of them. The value of P is the ratio of the soil losses by contouring or contour stripcropping to up-and-down-hill cultivation.

Contouring implies that tillage operations and row grades are close to the true contour. It is most effective on slopes in the 2 to 7 percent range. As land slope decreases, the effectiveness of contour farming approaches equality with contour grades and the soil-loss ratio becomes 1.0. As slope increases, contour row capacity decreases and the soil-loss ratio again approaches 1.0. Contouring alone will afford adequate

protection against low to moderate intensity storms, but not against severe storms. For this reason, terraces and diversions are frequently used in conjunction with contouring.

P factors for contour farming and contour striperopping are included in Table 14 together with limits for the application of these practices. Contour striperopping implies a crop rotation with alternate strips of cultivated row crops grown adjacent to strips of small grain or grass. When comparing soil losses from a system including contour striperopping with a system of contour farming or up-and-down-hill farming, remember the C factor in the striperopping system may change. For example, you cannot use the same C factor to compare continuous soybeans on the contour with soybeans contour striperopped because the striperopped soybeans are in a rotation with small grains or a sod crop while the contoured soybeans are not.

Terraces reduce soil loss by breaking long slopes into a series of short ones. The spacing of terraces by means of the Universal Soil Loss Equation is determined by solving for the LS factor. Terraces intercept and hold in the field most, but not all, of the soil lost in the interval between terraces. Because some soil can be expected to leave a terraced field, a value of 20 percent of the contour P factor is used when estimating watershed sediment yields but not when estimating other soil losses.

#### COMPUTING C FACTORS

The following information must be considered simultaneously when computing a C factor.

- 1. The distribution of erosive rainfall during the crop year.
- 2. The crops grown and the crop management used including individual crop characteristics, crop sequences, tillage times and methods, planting and harvesting dates, yields, crop residues, and crop residue management.

The pattern of erosive rainfall in a year varies throughout the country and within the state. The distribution is usually presented as a set of numbered graphs known as "Erosion Index Curves" or "EI Curves." The three curves used in Arkansas have been adjusted to county boundaries and are shown in Figure 2. The curves are presented in tabular form in Table 2. The percentage of the annual erosive rainfall that is expected within any particular crop stage period may be found by reading the number at the last and first date of the period and subtracting.

EI Curves are related to R values, but neither R nor EI values indicate the total amount of rainfall in a locality. R values represent the annual value of erosive rainfall; EI values the distribution of that rainfall.

# Cropstage Periods 1/

The change in effectiveness of plant cover within the crop year is gradual. For practical purposes, the year is divided into a series of cropstage periods defined so that cover and management effects may be considered approximately uniform within each period.

Initially, five periods were used, with the seedling and establishment periods defined as the first and second months after crop seeding (50). Because of the existing ranges in soil fertility, row spacing, plant population, and general growing conditions, however, soil loss prediction accuracy is improved when the cropstage periods are defined according to percentage of canopy cover rather than for uniform time periods. The lengths of the respective periods will then vary with crop, climate, and management and will be determined by conditions in a particular geographic area.

The soil loss ratios presented in the next subsection for computation of C were evaluated for six cropstage periods defined as follows:

Period F (rough fallow) - Inversion plowing to secondary tillage.

Period SB (seedbed) - Secondary tillage for seedbed preparation until the crop has developed 10 percent canopy cover.

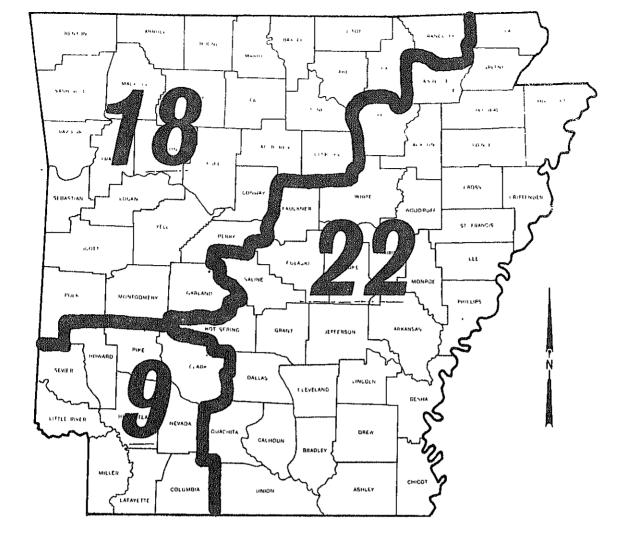
Period 1 (establishment) - End of SB until crop has developed a 50 percent canopy cover. (Exception: period 1 for cotton ends at 35 percent canopy cover.)

Period 2 (development) - End of period 1 until canopy cover reaches 75 percent. (60 percent for cotton.)

Period 3 (maturing crop) - End of period 2 until crop harvest. This period was evaluated for three levels of final crop canopy.

Period 4 (residue or stubble) - Harvest to plowing or new seeding.

1/ For detail discussion of crop canopy and residue mulch, see pages 18 and 19 of Agriculture Handbook Number 537.



# ARKANSAS

Figure 2 Erosion – Index

E

Distribution Curves

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Table 2

Distribution of Kainfall Erosion Indexes (E. I. Curves)
in Arkansas

Dates	Curve Number 9 18 22		Curve Number 18 22
1 Jan 1	0 0 0	30	54 50 55
10	1 1 2		57 54 59
20	2 2 4		59 58 63
2 Feb 1	4 3 6	8 Aug 1	62 63 67
10	5 4 8	10	64 61 70
20	7 5 <b>1</b> 0	20	67 70 73
3 Mar 1	9 6 13	9 Sep 1	70 74 75
10	12 8 16	10	72 77 77
20	14 9 19	20	75 80 79
4 Apr 1	16 10 22	10 Oct 1	78 84 81
10	20 13 25	10	80 87 82
20	24 16 30	20	83 90 84
5 May 1	28 19 33	11 Nov 1	85 92 86
10	34 24 37	10	88 94 88
20	38 29 41	20	90 96 91
6 Jun 1 10 20	42 35 44 46 40 48 50 45 52	12 Dec 1 10 20 30	93 92 94 95 98 96 98 99 98 100 100 100

#### PROCEDURE FOR DEVELOPING LOCAL "C" VALUES

Factor C in the USLE measures the combined effect of all the interrelated cover and management variables and is defined as the ratio of soil loss from land cropped under specified conditions to the corresponding loss from clean-tilled continuous fallow. It is usually expressed as an annual value for a particular cropping and management system. Soil loss ratio, as used in table 5, 1/express a similar ratio for a short time interval within which cover and management effects are relatively uniform. The cropstage soil loss ratios must be combined in proportion to the applicable percentages of EI to derive annual C values.

To compute the value of C for any particular crop and management system on a given field, one needs first to determine the most likely seeding and harvest dates, rate of canopy development, and final canopy cover. Also, the system to be evaluated must be carefully defined with regard to crop and residue management details. Within the broad limits of tables 5 and 6, these tables then supply the research data needed to complete the computation of C. The procedure will be explained by an example that, for illustration purposes, was selected to include many changes in field conditions.

It is not possible to include "C" values for all cropping situations. Table 10 list a number of alternative "C" values. The important factors that effect the "C" value are:

- 1. How much crop residue is produced.
- 2. How is the residue managed? Is it buried? If so when? What percent of the ground remains covered after planting?
- 3. How long does it take for the growing crop to produce an effective canopy? This will vary with the kind of crop, soil fertility and row spacing.

For more information on developing C values, see Agriculture HB 537, pages 29 and 30.

1/ See page 22 Agriculture HB 537.

# C FACTOR WORKSHEET

COUNTY	DATE	PREPARED BY	
50-100 bu. Rice 60	000-8000 lbs. *** 20-30	Oats 3000 lbs4000 lbs. *** bu. Soybeans 3000-5000 lbs. ** 0-100 bu. Corn 4000-6000 lbs. lbs. *** 30-40 bu. Wheat 4000-	
Date	: Percent : Percent : Canopy : Mulch	::::::::::::::::::::::::::::::::::::::	op Year C

Table 3 Assumed Mean Dates for Crop Stage Periods\*

	EI Curve	<i>०</i> / श्र	22 Counties	EI Cur	Curve 18 Counties	ties
,	Crop	Stage Peri	spo	Crop	Stage Peri	spc
Crops	(Start of seedbed	(Plant- (H ing or	(Harvest or graz-	(Start of seedbed	of (Plant- (Hant- or	(Harvest or graz-
Alfalfa	$\frac{\text{preparation}}{9/1}$	date) 10/1	1ng dave) 5/1	8/20	9/20	1118 dave /
Annual summer forages	(v)	, ,	00/0	٠, ٠,	۲/ ۵	1/8
Millet Guden ond Southum.	4/20		0/50	т/+	7 /C	7/0
Sudan Hybrid	14/20		8/20	14/1	5/1	8/1
Annual Lespedeza	2/1		9/1	2/1	2/10	1/6
Bahiagrass	3/1		다/8	3/1	4/1 	دا بر دا در
Bermudagrass	3/1		8/1	3/1	4/T	8/1 5/70
Corm, grain	3/10 3/10	4/50 14/50	10/20	3/10 3/10	↑/ <del>↑</del>	07/70 8/1
Cotton	3/10		10/20	3/10	5/1	10/20
Fescue, fall	9/1		11/10	9/1	10/1	11/10
Fescue, spring	2/20		01/11	1	1 (	15
	9/10		6/1	9/1	10/1	6/1 7/2
Oats, winter (grazing)	1/6		7/T	0/20	2/10 2/10	1/9 1/9
Orchardgrass, fall	8/20 20		11/10	8/15	9/15	01/11
	2/10		01/11	2/10	3/1	01/11
Peanuts	3/10		10/1	3/10	5/10	10/10
Rice	3/10		T/\T	3/10	4/20 5/4	T // L
Rye, grazing	9/1		2/1 2/1	02/0	7,0	T/C
Ryegrass	7/1		2/1	0/s/o	-1 ( 5), i	1/2
	T/1		10/1	4/T	01/C	τ / σ
Sorghum, Silage	4/1		0/7	4/+ 7-/-0	7/17	7/50 7/01
Soybeans	2/ TO		77/57	2/ 70	2160	707
Soybeans, after	(110		01/11	01/3	01/9	77/50
small grain	0/10		CT / T	0/ الم 1/0	07/0 1/01	6/10
Wileau 	51/5		A+ /A	1/0	10/12	) f
Winter cover crop	T/0T			7/07	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	

\*Incer cover crown and the state of the stat

Table 5

Ratio of Soil Loss from "No-Till"
to Corresponding Loss from Continuous Fallow

Line No.	Crops and Amounts of Residues (Lbs. per Acre)	Corn Yield Bu.		crop S	tage	
	Corn after corn planted <u>in</u> various amounts of <u>corn</u> residues.					
1 2 3 4 5 6	1,000 - 1,500 1,500 - 2,000 2,000 - 3,000 3,000 - 4,000 4,000 - 6,000 6,000 plus	75+	50 40 30 20 7 3	40 32 24 16 7 3	25 18 14 9 7 3	30 25 20 15 7 3
	Corn (for silage or grain) planted in various amounts of small grain residues.					
7 8 9 10	1,000 - 1,500 1,500 - 2,000 2,000 - 3,000 3,000 - 4,000 4,000 plus	75+	25 13 7 3	24 13 7 3 2	14 13 7 3 2	844 844 1046 844
	Corn after corn planted in sod.					
12 13	2,000 - 3,000 3,000 plus	75+	2	2	2	 
	Corn after corn planted <u>in rye-</u> grass.					
14 15 16	2,000 - 3,000 3,000 - 4,000 4,000 plus	75+	7 3 2	7 3 2	7 3 2	1 1 3
	Small grain after row crop in various amounts of residue after discing.					
17 18 19 20 21	500 - 750 750 - 1,000 1,000 - 1,500 1,500 - 2,000 2,000 plus		80 48 25 13 8	50 30 16 8	7 7 7 3 2	1 1 1 2 1

Table 6

Probabilities and Magnitudes of Brosion Indexes

	<b>်</b>	20 years	24 101 101 100 100 100 100 100 100 100 10	eri CV	rd el	
udec TIL	Index Values Normally Exceeded Once in	JO years	132 878 132 132	co CO	135	
Expected Magnituded of Jingle-Storm Erosion Index Values		years	101 115 68 105	5	다 다 다	
		ex Value	ex Value:	2 years	7,667	Ę,
	Inde	year	33 443	-1 <sub>1-3</sub>	57	
	5% Probability	(1 year out of 20)	614 569 432 600	536	658	
y Values Index	20% Probability	(l year out of 5)	400 7,22 301 301	384	493	
Probability Values of <u>Brosion Index</u>	50% Probability	(l year out of 2)	2514 308 325 325	272	365	
	Locations		Arkensas Ft. Smith Little Rock Mt. Home Texarkena	Tennessee Memphis	Mississippi Vicksburg	

## HOW TO USE THE SOIL LOSS EQUATION

#### CROPLAND

Example 1. A field of Calloway silt loam in St. Francis County has a slope length of 400 feet and gradient of 1.0 percent. The field is used for the production of continuous soybeans with conventional tillage methods. The average annual yield is 25 bushels per acre. The rows are run up and down the slope.

# How to estimate average annual soil loss from this field

- 1. Determine R value from Figure 1 for St. Francis County (R = 300).
- 2. Determine K and T values from Table 8 for Calloway silt loam (K = .49) and T = 3).
- 3. Determine IS factor from Table 9 for slope length of 400 feet and gradient of 1.0 percent (IS = .19).
- 4. Determine C factor from Table 10 for continuous soybeans, conventional tillage and average yield of 25 bushels per acre (C = .500).
- 5. Determine P value for up and down hill farming from Table 14 (P = 1.0).
- 6. Set up the equation A = RKISCP; insert the appropriate values and solve for A.
  - $A = 300 \times .49 \times .19 \times .500 \times 1$
  - A = 13.96 tons per acre average annual soil loss.

A quicker method is to refer to the appropriate RKLSP table in the appendix - the one with R=300 and K=.49. Locate slope length (400 feet) across the top and the percent of slope (1.0) along the left side. Move horizontally to the right from 1.0 percent and vertically down from 400 feet and take a reading where the two intersect. This is the RKLSP value - 27.93. Multiply this figure by the C factor (.500).  $A=27.93 \times .500 = 13.96$  tons per acre.

The maximum allowable soil loss for Calloway silt loam is three tons per acre per year. Therefore, this system of farming does not provide adequate protection.

If the rows are planted on the contour instead of up and down the hill the soil loss would be:

 $A = 300 \times .49 \times .19 \times .500 \times .6 = 8.37$  tons per acre.

To determine the soil loss using the appropriate RKLSP table, use the one with R=300, K=.49, rows up and down the hill. The RKLSP value for a 1.0 percent slope 400 feet long, rows run up and down the hill (P = 1.0) is 27.93. To complete the problem, multiply the RKLSP factor x P factor x C factor. A = 27.93 x .6 x .5 = 8.37 tons per acre. The P value for contour cultivation (from Table 14) for 1 percent slope is .60. 8.37 tons per acre still does not meet the minimum requirement - T = 3.

If the field is used for the continuous production of soybeans with no-tillage and rows up and down the hill, the C factor would be .100.

 $A = 300 \times .49 \times .20 \times .100 \times 1 = 2.94 \text{ tons.}$ 

This system should provide adequate protection as the projected average annual soil loss of 2.94 tons per acre is lower than the T factor of 3.

#### CONSTRUCTION SITES

Example 2. A shopping center is being built in Cleburne County on Linker fine sandy loam with 2 to 6 percent slopes. Figure 1 shows Cleburne County has an R value of 300. A parking lot has been graded and will be left unprotected until the adjacent buildings are completed.

#### How to estimate soil loss from this site

- 1. Determine the depth of the horizon exposed and its K value. Assume this site was cut 18 inches and the surface graded to a 2 percent slope 600 feet long. The K value for the 10 to 25 inch horizon of this soil is .32 (Table 8) and the LS value is .34 (Table 9).
- 2. There is no cropping system involved and the area will not be contour cultivated. The C factor is 1.0 and the P factor is 1.0.

 $A = R \times K \times LS \times C \times P$  $A = 300 \times .32 \times .34 \times 1 \times 1 = 32.64$  tons per acre per year.

The rate of soil loss may be found quicker by using the appropriate RKLSP table - the one with R=300 and K=.32, rows up and down the hill. Determine the value for a 2 percent slope 600 feet long. The value is 32.64. Multiply 32.64 by C value (1.0). A=32.64 x 1=32.64 tons per acre

To convert tons of soil to cubic yards lost, multiply the tons by the appropriate conversion factor from Table 7. The texture of Linker soil at the 18-inch depth is sandy clay loam and the conversion factor is 1.02. So 32.64 tons times 1.02 = 33.3 cu. yds.

#### PERIODS LESS THAN ONE YEAR

#### How to estimate soil losses for periods of less than one year

Example 3. A farmer in White County has plowed and prepared a seedbed for soybeans on March 10. The field has a 4 percent slope that is 200 feet long and has not been terraced. The soil is Linker fine sandy loam. How much soil loss can be expected from March 10 until soybeans are planted on May 20. Assume a crop history of continuous soybeans and a C value equal to .500.

- 1. Proxime the average annual soil loss expected.

  1. Proxime the average annual soil loss expected.

  2. Proxime the average annual soil loss expected.

  3. Proxime the average annual soil loss expected.

  4. Proxime the average annual soil loss expected.

  5. Proxime the average annual soil loss expected.

  5. Proxime the average annual soil loss expected.

  6. Proxime the average annual soil loss expected.

  6. Proxime the average annual soil loss expected.

  7. Proxime the average annual soil loss expected.

  8. Proxime the average annual soil loss expected.

  9. Proxime the average annual soil loss expected.

  9. Proxime the average annual soil loss expected.

  9. Proxime the average annual soil loss expected.
- In the County is number 22. Next, refer to Table 2 and find the percent of erosive rainfall for March 10 and May 20 under Curve 12. They are 16 and 41 respectively, a difference of 25. In indicates that 25 percent of the average rainfall erosive rain and 25 percent of the average annual soil loss may be expected during this period.
- 3. To estimate the soil loss, multiply the average annual soil loss by the percent of erosive rains for the period involved. The impact of losses =  $19.08 \times .25 = 4.77$  tons per acre.
- 4. The make procedure is used to estimate soil losses from construction sites. See Table 13 for C values.

#### THDIVIEWAL STORMS

#### How to estimate soil losses from individual storms

First obtain an adjusted R value from Table 18 page 54 in Agriculture HB 737. Also obtain an adjusted C value for the actual conditions that exist at the time of the storm by using Table 6 or 7 page 19 of Agriculture HB 537. The soil loss ratio will become the C value since no time factor is involved in a single storm. Proceed by using other factors in the equation.

Soil loss = RKLSCP, in the usual way.

This procedure cannot take into account the effects of antecedent moisture, tillage marks, compaction, soil crusting, etc., which affect soil erosion by water and which are not reasonably predictable. It is not as accurate as average long-term estimates, but it will provide reasonable estimates of single storm losses.

#### SOLL LOSS S LAREN EROSIVE RAINFALL EXCEEDS AVERAGE (SOIL LOSS PROBABILITIES)

### Ho to estimate soil losses other than the average

- Example 5. Refer to Example 1 where the <u>average</u> soil loss per year for a field in St. Francis County is 13.96 tons per acre when the field in Good for the continuous production of soybeans with conventional tillage and the rows run up and down the slope. To estimate the soil loss then crosive rainfall exceeds the average (or R value) and is equal to the maximum five-year frequency (20 percent probability or 1 year out of five) use the following procedure.
- 1. Refer to Table 6 and note that the value of EI for a 20 percent probability is 384 at Memphis, the location nearest St. Francis County for which records are available.

- 2. Find the value of an adjusted R by dividing the probability EI value by R. In this case, the adjusted R = 384 + 300 = 1.28.
- 3. Multiply the adjusted R by the average annual soil loss. The soil loss in the St. Francis County field is  $1.28 \times 13.96 = 17.86$  tons per acre in 20 percent of the years.
- 4. Similarly, losses in the same field for a 20-year frequency (5 percent probability) would be 536 + 300 x 13.96 = 24.56 tons per acre.

#### PASTURE, RANGELAND, IDLE LAND, AND WOODLAND

The procedure for estimating losses from pasture, idle lands, and woodlands are similar to that for cropland except that appropriate C factors are selected from Tables 11 and 12.

Table 7

Factors for Converting Tons
Per Acre to Cubic Yards Per Acre

Texture	Factor
Sands, loamy sands, sandy loams.	0.70
Sandy clay loams, silt loams, loams and silty clay loams.	0.87
Clay loams, sandy clays, clays and silty clays.	1,02

#### APPENDTX

#### CONTENTS

- Table 8. K and T Factors
- Table 9. LS Factors
- Table 10. "C" Factor Values for Cropland
- Table 11, "C" Values for Pasture, Range, and Idle Land
  Also Woodland Grazed, Burned or Recently Harvested
- Table 12. "C" Factors for Woodland
- Table 12A. "C" Factors for Mechanically Prepared Woodland Sites
- Table 13. "C" Factors for Annual Cover, and Various Quantities of Mulch
- Table 14. "P" Practice Factor Values

#### KRLSP Tables

TABLE 8
K AND T FACTORS
HYDROLOGIC GROUPS

SERIES	DEPTH	K <u>1</u> /	T 2/	HYDROLOGIC
	(Inches)	FACTOR	FACTOR	GROUP
Acadia	0-9	.43	4	D
	9-50	.32	-	-
Adaton	0-6	.43	5	D
	6-66	.37	-	
Agnos L CRL,CRSL	0-7 0-7	. 49 . 43	4 4	D D
Alaga	0-99	.17	5	A
Alamance	0-46	.43	4	В
Allegheny	0-9	.32	4	B
SIL	0-9	.28	4	- B
FSL	9-62	.28	-	-
Allen	0-12	. 24	5	B
	12-70	. 20	<del>-</del>	
Alligator	0~7	.32	5	D
C	0~7	.43	5	D
SICL	7~60	.24	<del>-</del>	-
Altavista	0-12 12-42	.20 .24	4 -	C
Amagon SIL FSL,SL	0-7 0-7 7-28 28-46 46-52	.43 .32 .43 .37 .43	5 5 - -	D D - -

<sup>1/</sup> Soil erodibility factor - a measure of rate at which a soil will erode.

 $<sup>\</sup>underline{2}$ / Soil-loss tolerance factor - permissable soil loss in tons per acre per year.

SERIES	DEPTH (Inches)	K 1/ FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP
Amy	0-18 18-68	.43 .43	5 -	D -
Angie	0-65	.32	3	С
Apison	0-8 8-40	.43 .37	3 -	B -
Arkabutla SIL	0-6 6-65	.37 .32	5 -	C -
Arkana CRV-SIL,SICL CR-SIL,CR-SICL SIL,SICL	0-11 0-11 0-11 21-27 27-29	.28 .32 .37 .24 .32	2 2 - -	C C - -
Ashton	0-9 9-80	. 28 . 43	4 -	D 
Ashwood	0-5 5-36	.43 .37	3	D
As kew	0-11 11-32 32-50 50-72	.37 .32 .24 .20	5  -	<u>c</u> 
Atkins	0-10 10-60	.43 .37	4 ~	D -
Augusta	0-9 9-65	.15 .24	4	B -
Barling	0-72	.37	5	С
Baxter	0-16 16-99	.32 .24	4 ~	B -
Beulah FSL,SL LFS,FS	0-8 0-8 8-40 40-60	.20 .17 .20 .17	5 5 -	B B -

SERIES	DEPTH (Inches)	K 1/ FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP
Bibb	0-37 37-60	.20 .37	5 -	C -
Blevins	0-72	.37	4	В
Boden	0-7 7-11 11-32 32-42 42-50	.24 .32 .28 .32 .24	3 - - -	C  
Bonn	0-64	.49	3	· Đ
Bosket	0-18 18-48 48-60	.24 .32 .24	4 - -	B 
Boswell SIL FSL	0-5 0-5 5-70	.43 .37 .32	5 5 -	D D 
Bowdre	0-20 20-52	.37 .32	5 -	<u>c</u>
Bowie	0-12 12-42 42-78	.24 .32 .28	4 	B 
Braddock	0-10 10-60	.20 .17	5 -	B -
Brandon	0-9 9-30 30-60	.37 .28 .17	3 -	B 
Brewer	0-12 12-50 50-90	.43 .37 .43	5 - -	C - -
Brocket GR-FSL,GR-SC,GR-L FSL,SL,L	0-16 0-16 16-58 58-72	.24 .28 .32 .24	5 5 -	C C -

	DEPTH	V 17		
	(Inches)	K 1/ FACTOR	T 2/ FACTOR	HYDROLOGIC
Britwater	0-6		170107	GROUP
	6-60	.32	3	
	60 <b>-</b> 74	. 28		В
<b>5</b>	00-74	.24	•	~
Broseley	0-37	_		••
ь	0-47	.20	5	
Bruno	0-80	n	•	В
Description		.17	5	2
Buxin				А
SICL	0-6	20		
C,SIC	0-6	.32	5 5	<b>D</b>
	6-60	.28	5	D
Caddo		.32	-	D
Caudo	0-30	.43		~
	30-87	.37	3	D
Cahaba		.0/	No.	
Janaba	0-9	.24	ā	-
	9-53	.28	4	В
	53-80	,24	**	~
Calhoun	A N=	7 1	4	•
	0-17	.49	2	
	17-72	.43	3	D
alloway	0.20		<del></del>	-
	0-30	.49	3	
	30-60	.43	J	C
ane	0~5		-	<b>~</b>
	5-75	.32	3	
	3-75	.37	<b>™</b>	В
aptina	0-14			<b>L.</b>
	14-24	.43	3	•
	24-60	.37	-	C
	, 00	.32	m	<b>u</b>
rnasaw	0-9	40		bar
	9-15	.43 .37	3	С
	15-42	.32	M	
rytown		. 32	-	<b>-</b>
y cown	0-15	.43	_	
scilla		170	2	D
Cilia	0-72	.43		D
piana		1-10	5	В
ICL				
IL	0-11	.32	e e	
w	0-11	.37	5 5	В
	11-60	.32		B B
alpa	0.00		-	~
1 =1	0-60	.28	Λ	
			4	C

SERIES	DEPTH (Inches)	K <u>1</u> / FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP
Ceda	0-55	.28	5	В
Chastain	0-10 10-72	.32 .37	5 -	D -
Chenneby	0 <b>-</b> 55 55-72	.32 .24	5 -	<u>c</u>
Cherokee	0-15	.43	4	D
Chewacla SL,FSL SIL,L SCL,L,SL SIL,CL,SICL	0-14 0-14 14-58 14-58 58-70	.24 .28 .28 .32 .32	5 - - -	C   
Christian	0-6 6-65	.37 .28	3 -	C -
Clarksville	0-80	.24	2	В
Cleora L,FSL LFS	0-15 0-15 15-70	.32 .17 .32	5 5 -	B  -
Collins	0-48	.43	5	В
Commerce SICL SIL,L,VFSL	0-10 0-10 10-36 36-60	.32 .37 .32 .37	5 5 - -	C C -
Conasauga	0-4 4-10 10-30	.43 .32 .32	2 -	C - -
Congaree	0-80	.37	5	В
Convent	0-60	.37	5	С

SERIES	DEPTH (Inches)	K 1/ FACTOR	T 2/ FACTOR 2/	HYDROLOGIC GROUP
Corydon (See Arkana	Series)			
Coushatta SIL,VFSL SICL	0-8 0-8 8-27 27-61	.37 .32 .32 .37	5 5 -	B B -
Craig SIL,L CR-SIL,CR-L	0-16 0-16 16-21 21-60	.37 .32 .32 .28	3 3 - -	C C -
Crevasse	0-60	.15	5	Α
Crowley	0-16 16-60	.43 .32	4	D 
Culleoka SIL FSL,SIL	0-9 0-9 9-27 27-33	.32 .28 .28 .17	3 3 	B B -
Dardanelle	0-23 23-91	.37 .32	5 	B ~
Davidson	0-7 7-12 12-53 53-73	.28 .32 .24 .28	5 - - -	B  
Demopolis L,CL,SIL GR-SIL,GRL,GR-CL	0-6 0-6 6-12 12-48	.37 .32 .32 .24	]	C C - -
Desha SIL,SICL SIC,C	0-7 0-7 7-44 44-72	.43 .32 .28 .37	5 5 -	D D -

SERIES	DEPTH (Inches)	K 1/ FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP
Dexter	0-6 6-32 32-67	.37 .32 .24	5	B 
Doniphan	0-12 12-77	.32 .28	4 -	B -
Dubbs SIL SICL	0-5 0-5 5-50	.37 .32 .37	5 5 -	B B
Dundee	0-56	.32	5	С
Dunning	0-15 15-72	.37 .28	3	D -
Earle SICL C,SIC	0-6 0-6 6-29 29-60	.37 .32 .37 .43	5 5 -	D D - -
Egam	0-56 56-75	.32 .37	4 -	C -
Elk	0-9 9-69	.32 .28	4 -	C -
Elsha	0-10 10-60	.32 .24	4 -	В
Emory	0-60	.37	5	В
Enders VFSL,SIL GR-VFSL	0-5 0-5 5-8 8-62	.37 .32 .43 .37	3 3 -	C C -
Ennis	0-60	.28	5	В
Etowah	0-7 7-70	.37 .32	5	В

SERIES	DEPTH (Inches)	K <u>1</u> / FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP
Eutaw SIL SICL	0-9 0-9 9-82	.37 .32 .28	5 5 -	D D ~
Falaya	0-65	.43	5	D
Faulkner	0-21 21-65	.43 .24	4 -	C -
Fatima	0-67	.37	5	В
Fayetteville ST-FSL,ST-L SL,FSL	0-9 0-9 9-16 16-67	.20 .24 .24 .32	4 4 	B B ~ -
Foley	0-8 8-42 42-60	.43 .43 .49	3	D 
Forestdale	0-6 6-48	.43 .28	5 -	D 
Fountain	0-75	.37	3	D
Gallion SICL SIL	0-10 0-10 10-44 44-60	.32 .37 .32 .37	5 5 -	B ~ -
Gassville CR-SIL CRV-SIL	0-11 0-11 11-19 19-50	.43 .37 .32 .37	3 3 -	C C -
Georgeville	0-7 7-3 <b>4</b> 34-45	.43 .37 .43	3 -	B 

SERIES	DEPTH (Inches)	K <u>1</u> / FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP
Gepp GR-SIL SIL	0-7 0-7 7-12 12-75	.32 .37 .32 .28	4 4 ~ ~	B B 
Goldsboro	0-15 15-76	.20 .24	5 -	B -
Goldston	0-18	.20	2	С
Gore	0-5 5-73	.43 .32	3 -	D -
Greenville	0-6 6-72	. 24 . 17	5 -	B 
Grenada	0-24 24-60	.43 .37	3	C -
Grubbs	0-5 5-27 27-60	.49 .37 .49	5 - -	- -
Guin	0-60	.37	4	В
Guthrie	0-68	.43	5	D
Hanceville	0-8 8-54 54-63	.24 .28 .24	3 -	B ~ ~
Hartsells	0-13 13-36	.28 .32	2	B ~
Hayti FSL	0~6 6~72	.32 .37	5	D 
<b>Healing</b>	0-60	.37	5	В
Hebert SICL SIL,VFSL	0-10 0-10 10-37 37-72	.32 .37 .32 .37	4 4 -	C C -

SERIES	DEPTH (Inches)	K ]/ FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP
Hector	0-15	.17	1	D
Henry	0-60 60-90	.43 .49	5 -	D 
Herndon	0-9 9-48 48-68	.43 .37 .43	3 - -	B 
Hillemann	0-15 15-23 23-60	.49 .43 .49	3	C - -
Hollywood	0-4 4-72	.32 .37	3 -	D -
Ho1ston	0-74	.32	5	В
Hontas	0-72	.37	5	В
Houston	0-10 10-72	.37 .32	4 -	D <del>-</del>
Huntington	0-11 11-60	.37 .43	5 -	B -
Iuka LS FSL,L	0-13 0-13 13-22 22-60	.17 .24 .28 .20	5 5 -	C C - -
Izagora VFSL,FSL L,SIL	0-11 0-11 11-91	. 28 . 37 . 32	4 3	C C -
Jackport	0-5 5-46 46-65	.43 .32 .43	5 - -	D  -
Jay	0-16 16-29 29-72	.43 .37 .32	3 - -	c - -

SERIES	DEPTH	K <u>1/</u>	T 2/	HYDROLOGIC
	(Inches)	FACTOR	FACTOR	GROUP
Jeanerette	0-6	.32	3	C
SICL	0-6	.37	3	C
SIL	6-60	.32	-	-
Jefferson	0-43 43-65	.28 .17	4	B -
Johnsburg	0-19 19-56 56-70	.43 .37 .32	3	D 
Kalmia	0-14	.20	4	B
	14-32	.24	-	-
	32-60	.10	-	-
Kaufman	0-72	.32	5	D
Keo	0-56	.37	5	В
Kipling	0-3	.43	4	D
SIL	0-3	.32	4	D
SICL	3-62	.32	-	-
Kirvin	0-11	.37	4	C
	11-64	.32	-	
Kobel SIC SICL SIL	0-5 0-5 0-5 5-72	.37 .43 .49 .37	5 5 5	D D D
Lafe	0-60	.49	1	D
Lagrange	0-33	.24	5	<u>م</u>
	33-72	.37	-	-
Latanier	0-6	.37	5	D
	6-30	.32	5	D
	30-60	.37	-	

SERIES	DEPTH (Inches)	K 1/ FACTOR	T 2/ FACTOR	TIY DROILOG1C GROUP
Latonia FSL LS	0-4 0-4 4-32 32-74	.20 .17 .20 .17	4	B C -
Leadyale	0-48 48-58	.43 .24	3 -	C -
Leaf	0-9 9-72	.32 .32	3 -	D ~
Leeper	0-50	.28	4	D
Leesburg	0-6 6-65	.24 .32	5 -	B -
Lexington	0-38 38-65	.49 .24	4	B -
Lindside	0-17	.37	4	В
Linker FSL,L,GR-FSL ST-FSL,ST-L	0-5 0-5 5-10 10-25 25-35	.24 .20 .24 .32 .28	3 3 	B B  -
Lobelville	0-65	.28	5	В
Locust	0-64 64-70	.37 .28	3 -	C -
Lonoke	0-32 32-60 60-80	.24 .28 .24	5 - -	B 
Loring	0-65	.43	3	С
Lucy	0-24 24-35 35-70	.17 .24 .28	5 - -	B 

SFRIES	DIPIH (Inches)	K 1/ FACTOR	r 2/ FACTOR	HYDROLOGIC GROUP						
Luverne	0-5 5-41	.37 .28	3	C -						
Mantachie	0-61	. 28	5	С						
Marietta	0-62	.28	5	r						
Marvell	0-36 36-60	.24 .37	5	B -						
Mashu <b>la</b> ville	0-26 26-62	.32 .28	4 -	D -						
Mayes	0-14 14-60	.49 .43	5 <del>-</del>	D ~						
Mayhew	0-7 7-80	.37 .32	5 <del>-</del>	D 						
McCroy	0-15 15-27 27-52	. 24 . 32 . 49	3 ~	D •						
McGehee	0-17 17-24 24-60	.43 .37 .32	5 -	C 						
<b>M</b> cKamie	0-5 5-36 36-60	.43 .32 .37	3	D - -						
Mecklenburg FSL GR-L	0-6 0-6 6-36	.28 .24 .32	4 4 	D D -						
Melvin	0-60	. 43	5	D						
Memphis	0-77	.37	5	В						
Mhoon SICL SIL	0-6 0-6 6-60	.37 .43 .37	5 5 -	D D						

SERIES	DEPTH (Inches)	K <u>1/</u> FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP
Millwood	0-7 7-72	.49 .37	5 -	D 
Moko	0-10	.32	1	D
Monogahela	0-12 12-50	.43 .37	3 ~	C ~
Montevallo	0-16	.37	2	D
Moreland SIL SICL C	0-10 0-10 0-60	.43 .37 .32	5 5 5	D D D
Morganfield	0-50	.43	5	В
Morse	0-60	.37	4	D
Mountainburg	0-6 6-18	.17 .24	1 -	D -
Muldrow SICL, CL SIL	0-18 0-18 18-70	.43 .49 .43	5 5 -	D D -
Musella GR-CL,GR-L CL,L	0-4 0-4 4-18	.28 .32 .32	2 2 	С С
Muskogee	0-14 14-26 26-72	.43 .37 .32	5	C - -
Myatt	0-10 10-50 50-72	.32 .28 .24	5	D 
Nacogdoches	0-80	.32	5	С
Natchez	0-65	.37	5	В

SERIES	DEPTH (Inches)	K 1/ FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP
Nella	0-14 14-70	.20 .17	5	В
Newark	0-9 9-60	.43 .43	5 ~	B -
Newellton	0-5 5-14 14-60	.37 .32 .37	5 - -	D 
Newtonia L,SIL SICL	0-9 0-9 9-18 18-61	.37 .32 .37 .32	5 5 -	B B -
Nixa	0-32 32-35	.43 .37	2 -	C -
Noark	0-10 10-17 17-70	. 32 . 28 . 24	3 - ~	B 
Norfolk	0-17 17-80	.17 .24	5	B 
Norwood SIL SICL	0-11 0-11 11-60	. 43 . 32 . 43	5 5	8 8
Nugent	0-60	.17	5	А
Ochlockonee	0-44 44-72	.20 .17	5 ~	B -
Oklared SICL FSL,VFSL,L	0-10 0-10 10-60	.28 .32 .32	5 5 ~	B B
<b>O</b> ktibbeha	0-70	.32	3	D

SERIES	DEPTH (Inches)	K ]/ FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP
Ora	0-7 7-26 26-56	.32 .37 .32	3 - ~	C - -
Orangeburg LS,LFS SL,FSL	0-7 0-7 7-64	.20 .24 .24	5 5	B B 
Ouachita	0-19 19-69 69-77	.37 .32 .24	5 - -	C  
Ozan	0-15 15-72	.32 .43	5	D -
Paron	0-9 9-56 56-72	.24 .28 .24	4	B 
Parsons	0-12 12-80	.49 .43	4 ~	D ~
Patterson FSL LFS	0-9 0-9 9-32 32-52	.20 .17 .20 .17	5 5 -	C C -
Pembroke	0-9 9-96	.32 .28	4 -	<u>c</u>
Peridge	0-8 8-42 42-54 54-74	.37 .32 .28 .24	5 - -	B - -
Perry SICL C,SIC	0-6 0-6 6-60	.32 .24 .28	5 5 	D D -
Pheba	0-21 21-60	.49 .43	3 -	C -

SERIES	DEPTH (Inches)	K 1/ FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP
Philo	0-40	.37	5	В
Pickens	0-17	.28	2	<b>"</b> D
Pickwick	0-6 6-80	. 43 . 37	5 -	B
Pineville	0-13 13-45 45-56	.17 .20 .15	3 -	B 
Pirum	0-11 11-36	.24 .32	3 -	<u>B</u>
Pledger	0-70	.32	5	D
Pope	0-85	.28	5	В
Porters	0-7 7-28	. 24 . 24	4 -	B 
Portia	0-10 10-24 24-46 46-72	.24 .37 .32 .28	3 - -	C  
Portland SIC,C SIL	0-8 0-8 8-65	.32 .43 .32	5 5	D D ~
Prentiss	0-73	. 24	3	С
Providence	0-23 23-60	.43 .32	3 -	C
Pulaski FSL,L LFS	0-10 0-10 10-64	.32 .17 .32	5 5	B B
Razort	0-54 54-60	.37 .32	5 -	B ~

SERIES	DEPTH (Inches)	K 1/ FACTOR	T 2/ FACTOR	HYDROL OG I C GROUP
Rexor	0-70	.37	5	А
Rilla	0-8 8-69	.37 .32	5	B -
Roanoke	0-7 7-50	.43 .32	4	D -
Robinsonville	0-70	.32	5	В
Roellen	0-14 14-72	.32 .37	5 -	D -
Roxana	0-70	.37	5	В
Ruston GR,FSL FSL,SL,LFS	0-16 0-16 16-41 41-47 47-92	.28 .32 .28 .32 .28	5 5 - -	8 B - -
Sacul	0-44 44-72	.32 .37	3	С -
Saffell GR-FSL,GR-SL FSL,SL,LFS	0-8 0-8 8-50 50-60	.20 .24 .28 .17	4 4 - -	B B -
Sallisaw	0-36 36-40	. 32 . 28	4 -	B -
Samba	0-6 6-12 12-66	.49 .43 .37	5  -	D 
Sardis	0-72	.37	5	С
Sayannah FSL SL	0-11 0-11 11-68	.37 .24 .28	3 3 -	C C

SERIES	DEPTH (Inches)	K 1/ FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP					
Sawyer	0-5 5-29 29-80	.43 .37 .32	3	C 					
Secesh	0-60	.37	4	В					
Sequatchie	0-72	.24	5	В					
Severn	0-60	.32	5	В					
Sharkey SIL SICL C	0-9 0-9 0-9 9-60	.43 .37 .24 .28	5 5 5	D D D					
Sherwood	0-12 12-38 38-50	.37 .32 .28	3 - -	B - -					
S <b>hub</b> uta	0-8 8-70	.37 .28	3 -	C -					
S1oan	0-60	.37	5	В					
Smithdale Fsl LS	0-11 0-11 11-60	.28 .17 .24	5 5 	В В -					
Smithton	0-72	.32	5	Ð					
Sogn	0-9	.32	1	D					
Spadra	0-39 39-72	.37 .24	5 <del>-</del>	B ~					
Staser	0-52	.32	5	В					
State	0-60	.42	5	В					
Steele	0-28 28-48	.20 .32	5 -	C					

SERIES	DEPTH (Inches)	K 1/ FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP					
Stendal	0-55	.37	5	В					
Sterlington	0-60	.37	5	В					
Stough	0-20 20-68	.28 .37	3 -	<b>c</b>					
Stuttgart	0-22 22-31 31-45 45-60	.43 .32 .37 .43	3 - - -	D  					
Summit	0-18 18-60	.37 .32	4 ~	c -					
Sumter	0-30	.37	3	С					
Susquehanna FSL,SL,SIL,L LS	0-5 0-5 5-77	.43 .17 .32	3 3 -	D D 					
Taft	0-64 64-80	.43 .37	4 -	- C					
T <b>al</b> oka	0-28 28-78	.49 .43	5 	D 					
Tate	0-7 7-38	.24 .28	4 -	B -					
Terouge	0-72	.32	5	D					
Tiak	0-8 8-26 26-68	.32 .37 .32	4 - -	C - -					
Tichnor	0-36 36-65	.43 .37	5 -	D -					
Tippah	0-31 31-60	.43 .24	4 -	C -					

SERIES	DEPTH (Inches)	K 1/ FACTOR	T <u>2</u> / FACTOR	HYDROLOGIC GROUP
Tiptonville	0-12 12-72	.32 .28	5	B 
Toine L,SIL FSL	0-13 0-13 13-55 55-72	.37 .24 .32 .24	3 3 -	C C -
Tonti	0-6 6-29 29-42	.37 .32 .28	3 - -	C - -
Townley	0-6 6-22	.37 .32	2	C -
Trebloc	0-65	.37	3	D
Trinity	0-80	.32	5	D
Troup	0-40 40-99	.17 .20	5 	-A
Tuckerman	0-18 18-34 34-52 52-62	.24 .32 .24 .20	5 - -	D - -
Tunica	0-28 28-48	.32 .43	3 -	D -
Tuscumbia	0-50	.28	5	D
Tutwiler	0-24 24-48	.24 .17	4 -	B -
Una	0-57	.28	5	p
Vaiden	0-79	.32	4	D
Ventris	0-8 8-31	.43 .37	2 -	D -

SERIES	DEPTH (Inches)	K 1/ FACTOR	T 2/ FACTOR	HYDROLOGIC GROUP
Vicksburg	0-55	.43	5	В
Wabbaseka C,SIC SICL	0-18 0-18 18-42 42-80	.37 .43 .37 .2	5 5 -	D D -
Waben	0-15 15-66	.28 .24	5 ~	B -
Wardell	0-16 16-37 37-72	.43 .37 .32	4 - -	<u>c</u> -
Waverly	0-60	.43	5	D
Waynesboro	0-10 10-60	.24 .28	5 -	B -
Wehadkee	0-8 8-40 40-50	.24 .32 .28	5 -	D 
Weston LFS FSL,SL	0-9 0-9 9-44 44-54	.20 .24 .24 .32	5 - -	D - -
Wickham	0-7 7-40	.20 .24	5 ~	B 
Wilcox	0-5 5-57	.37 .32	4 -	D -
Wilson	0-6 6-80	.43 .37	5	D -
Wing SL SIL,L	0-5 0-5 5-60	.37 .49 .49	1 1 -	D D -

SERIES	DEPTH	K 1/	T 2/	HYDROLOGIC
	(Inches)	FACTOR	FACTOR	GROUP
Wrightsville SIL,SL SICL	0-16 0-16 16-50 50-66	. 49 . 43 . 37 . 43	5 5 -	D D ~
Yorktown	0-60	.32	5	D
Zachary	0-28	.49	5	D
	28-60	.43	-	

00.11 00.13 00.27 00.39 00.39 00.39 11.10 300. 00.11 00.13 00.26 00.37 00.37 00.37 11.56 00.84 00.85 00.85 00.86 00.86 00.87 00.85 250. 00.10 00.15 00.15 00.24 00.25 200-150. SNO ONE PAGE 140. SOIL LOSS EQUATION LS FACTORS SLOPE LENGTH IN FEET 100. 75. 50. 0.25 0.50 1.00 3.00 3.00 4.00 6.00 6.00 11

		2000-	0.20	0.24	0.31	0.49	0.70	1.32	2,39	3.00	3.68	4.43	5.24	6-12	7.06	8.07	9.13	10,26	24°	12.69	18.24	26.34	35,04	56.59	1005	103,54	126.97	149,27	169,99	ω	
		1600.	0.19	0.22	67.0	0.46	0.66	1-21	2.14	2.69	3.30	3.96	69.4	5.47	6.32	7.21	8.17	53.5	IC . 24	를 6 (건	₹ <b>6</b> -3¥	23.56	्र 8° ह€	50.51	F = 29	92.60	14	193	3	80	
		1200-	0-17	0.20	0.27	0.42	0.60	₹*08	± 85	2.33	2-85	3,43	4.06	42 - 4	2.47	6.25	7007	7.95	8 36	9.83	4	C	27.55	m	125	О	ന സ സ	L I	121.68	5.5	
	2E 140	1000.	0.16	0.19	0.25	0.40	25*0	1.00	1.69	2.12	2.60	3.13	3,71	4.33	4*99	5.70	6.46	7.25	8.09	26.8	N	18.62	25.15	40.03	56-36	73.21	89.78	105,55	120,20	33,59	
	S PAGE	800°	0.15	0-18	0.24	0.37	0.53	16.0	1451	1.90	2.33	2.80	3,31	•	4-46	5.10	2.12	6-49	7.24	8.03	11.53	16.66	22.49	35.79	50.41	65.48	80,30	94.41	107,51	119-49	
	SOIL LOSS EQUATION LS FACTORS SLOPE LENGTH IN FEET	700 <b>.</b>	0.15	0.17	0.23	0.36	0,51	0.87	1.41	1.78	2-18	2.62	3.10	3,62	4-18	4.77	5.40	6.07	6.77	7.51	10.79	15.58	21.04	33.47	47.16	61.25	75.12	03 03 04 04	100.57	111.77	
Table 9	S EQUATION PE LENGTH	•009	0.14	0.16	0.22	0.34	0-49	•	1.31	1.64	2-02	2.42	2.87	3-35	3.87	4.42	2*00	5-62	6.27	6*35	66*6	14.43	19.48	30.99	43.66	56.71	59.54	81.76	93.11	103.48	
	SOIL LOSS E	*005	0-13	0.16	0.20	0.32	0.46	92.0	1-19	1.50	1-84	2.21	2.62	3-06	3.53	4.03	4.56	5-13	5.72	6.34	9-12	13.17	17.78	28.29	39*85	, i	m	\$	84.99	94.46	
		450-	0.13	0.15	0.20	0.31	0.45	0.73	1.13	1.42	1,75	2.10	2.48	2.90	3,35	3.82	4.33	4.86	5.43	6.02	8-65	12,49	16.87	26.84	37.81	49.11	60.23	70.80	60.63	89.61	
		<b>*</b> 00 <b>*</b>	0.12	0.14	0.19	0.30	0.43	69-0	1.07	1.34	1.65	1.98	2,34	2-13	3.16	3.60	4.08	4.59	5.12	5.67	8.15	11.78	15.90	25.30	35.64	46.30	56.78	66.75	76.02	84.49	
		350.	0.12	0.14	0.18	0.29	14.0	0.66	1.00	1-25	1+54	1.85	2.19	2.56	2.95	3.37	3.82	4-29	4.79	5.31	7.63	11.02	14.88	23.67	33.34	43.31	53-11	62.44	71-11	79.03	
		PERCENT SLOPE	0.25	0*20	1.00	2*00	3-00	<b>4.</b> 00	2.00	9*00	7.00	8.00	00.6	10-00	11.00	12.00	13.00	14.00	15.00	16.00	20.00	25.00	30-00	<b>40.00</b>	50*00	00.09	70-00	80.00	90-00	100.00	// PAUSE

Table 10
Cropping Management Factors
(Average "C" Factor Values)
Arranged in Order of Effectiveness for Cropping Systems in Arlausas

Order	Cropping System	Yields per Acre	Average Annual "C" Value
1	Meadow, well established grass and legume. Excellent cover		.004
2	Meadow, well established grass and legume. Good cover	1-2 ton	.010
3	Meadow, well established, Sericea lespedeza		.010
14	Annual lespedeza - seed, rd.l.		.010
5	Orchard - Continuous cover. Annual lespedeza		.010
6	Annual lespedeza, well established. Hay or grazed	2 ton	.020
7	Continuous Corn, No-til, rd.1. Minimum residue 4,000 lbs./acre	70 bu.	.070
8	Continuous grain sorghum, No-til, rd.l. Residue minimum 4,000 lbs. per acre	4,000 lbs.	.070
9	Winter cover crop orchard. Minimum seedbed preparation. Mow about April and mow summer growth		.080
10	Soybeans (No-til) - Double cropped with small grain. Minimum seedbed preparation for small grain	Beans, 25 bu. Wheat, 35 bu.	<b>.0</b> 80
11	Soybeans - small grain, Soybeans, Rice. Soybeans and small grain No-til planted. Start seedbed pre-paration for rice after April 1		.100
12	Continuous Rice. Rd.1. Residue rolled soon after harvest. Seedbed preparation about March 1	100 bu.	.100
13	Continuous Soybeans, rd.1. No-til. Minimum 4,000 lbs. residue/acre	Beans, 30 bu.	.100

## Table No. 10 (Continued)

Order		Yields per Acre	Average Annual "C" Value
14	Rice, Rice, Soybeans. Rd.1. Prepare seedhed about one month before	Rice, 100 bu. Beans, 25 bu.	.J10
15	Corn rd.1. A. lespedeza, A. lespedeza. Corn residue av. 4,000 lbs. per acre, conventional tillage	Corn, 70 bu. A.lesp. 15 ton	.L10
16	Continuous Corn (silage). Residue 1,500 lbs./acre. Winter cover crop each year - grazed. No-til	Silage, J5 ton	.120
17	Continuous small grain, rd.l. Min- imum seedbed preparation immed- iately prior to planting	Wheat, 30 bu. Oats, 60 bu.	.120
18	Continuous Corn, rd.l. No-til. Average 3,500 lbs. residue/year	Corn, 50 bu.	.1.20
. 19	Continuous Soybeans, rd.l. No-til. Average 3,500 lbs. residue/year	Beans, 20 bu.	.120
20	Continuous grain sorghum, rd.1. No-til. Average 3,500 lbs. residue per year	Grain, 3,500 lbs.	.120
21	Small grain-Soybeans double cropped, broadcast, rd.l. Minimum seedbed preparation	Oats, 70 bu. Wheat, 35 bu. Soybeans, 25 bu	<b>.</b> L <sup>1</sup> 10
22	Continuous small grain, rd.l. Con- ventional seedbed preparation	Wheat, 30 bu. Oats, 60 bu.	.150
23	Corn, Corn, A. lespedeza, A. lespedeza. Minimum corn residue 4,000 lbs./acre. Conventional tillage	Corn, 60 bu. Lesp. 1½ ton	.150
24	Soybeans, Wheat, Soybeans, rd.1. Beans No-til planted. Seedbed for wheat light discing	Beans, 30 bu. Wheat, 40 bu.	.150
25	Rice, Rice Soybeans, rd.1. Pre- pare seedbed soon after harvest. Soybeans non-irrigated	Rice, 100 bu. Beans, 25 bu.	.170
26	Rice, Rice, Soybeans, Soybeans. Seedbed preparation delayed until after April 1. Both crops irrigated	Rice, 100 bu. Beans, 25 bu.	.190

Table No. 10 (Continued)

Order		Yields per Acre	Average Annual "C" Value
27	Soybeans-Wheat, Soybeans, Soybeans, Soybeans, Soybeans, Cotton. Soybeans "No-til." Prepare seedbed for wheat by light discing or with tiller leaving most of residue on soil surface. Prepare conventional seedbed for cotton after April 1.	Beans, 30 bu. Beans (after Wheat) 25 bu.	.190
28	Continuous Corn rd.l. Minimum seedbed preparation after March 15. No cultivation. Minimum residue 4,000 lbs./acre	Corn, 70 bu.	.190
29	Continuous Grain sorghum rd.1. Minimum seedbed preparation after April 1. No cultivation. Minimum residue 4,000 lbs./acre	Grain, 4,200 lbs.	,190
30	Continuous Soybeans rd.1. Minimum seedbed preparation after April 15. No cultivation. Minimum residue 4,000 lbs./acre	Beans, 25 bu.	.190
31	Continuous Soybeans, rd.l. "Stubble plant." Minimum cultiva- tion	Beans, 30 bu.	.200
32	Continuous Cotton, rd.l. "Stubble plant." Minimum cultivation	Cotton (lint) 500 lbs.	.200
33	Continuous Corn, rd.1. Minimum seedbed preparation after March 15. No cultivation	Corn, 70 bu.	.200
314	Continuous Grain sorghum, rd.1. Minimum seedbed preparation after April 1. No cultivation	Grain, 4,200 lbs.	.200
35	Rice, Rice, Soybeans, Soybeans, rd.1. Soybeans non-irrigated. Conventional seedbed preparation	Rice, 100 bu. Soybeans,25 bu.	.210
36	grain-Soybeans, rd.1. Conventional	Oats, 70 bu. Wheat, 35 bu. Beans, 20 bu.	.230

Table No. 10 (Continued)

Order	Cropping System	Yields per Acre	Average Annual "C" Value
37	Rice, Soybeans, Soybeans, rd.1. Both crops irrigated with levees. Conventional seed bed preparation	Rice, 100 bu. Beans, 25 bu.	.250
38	Continuous Corn, rd.1. Effective winter cover crop each year	Corn, 70 bu.	.260
39	Sudan (or hybrids) double cropped with small grain. Both crops fertilized and grazed. "No-til" planted	Sudan, 5 AUM Sm.grain 4 AUM	:260
40	Soybeans-small grain double cropped, rd.l. Conventional seedbed preparation	Beans, 25 bu. Wheat, 30 bu. Oats, 60 bu.	•300
41	Sudan (or hybrids) double cropped with small grain. Both crops well fertilized and grazed. Minimum seedbed preparation each crop	Sudan, 5 AUM Sm.grain 4 AUM	.300
42	Continuous Corn, rd.1. Effective winter cover crop every 2nd year. Conventional seedbed preparation.	Corn, 60 bu.	.300
43	Rice, Soybeans, Soybeans, Soybeans, rd.l. Conventional seedbed preparation and cultivation. Rice flood irrigated	Rice, 100 bu	.330
ЦĻ	Continuous Corn, rd.1. Conventional tillage. Prepare seedbed after March 15	Corn, 75 bu.	.330
45	Continuous Corn, rd.l. Effective winter cover crop every third year	Corn, 60 bu.	•350
46	Continuous Corn (silage). Effective cover crop each year. Conventional tillage	Silage, 15 ton	.350
47	Continuous Corn, rd.l. Effective cover crop each year. Conventional tillage	Corn, 45 bu.	.350

Table No. 10 (Continued)

Order	Cropping System	Yields per Acre	Average Annual "C" Value
1/8	Continuous Cotton, rd.l. High fer- tility. Effective winter cover crop each year. Conventional		
	tillage	Lint, 600 lbs.	.350
49	Continuous Soybeans, rd.1. Prepare conventional seedbed after April 1		.350
50	Continuous Soybeans, rd.1. Conventional tillage	Beans, 35 bu.	.350
51	Continuous Soybeans, rd.l. Effective cover crop each year	Beans, 20 bu.	.350
52	Continuous Cotton, rd.l. Effective winter cover crop each year	Lint, 450 lbs.	.350
53	Cotton, Cotton, Soybeans, Soybeans. Prepare conventional seedbed for cotton after April 1. Soybeans, no-til	Lint, 600 lbs. Beans, 30 bu.	.350
54	Continuous Corn, rd.l. High fertility. Conventional seedbed preparation	Corn, 75 bu.	.350
55	Continuous Corn, rd.1. Winter cover crop every 2nd year. Conventional tillage.	Corn, 45 bu.	.400
56	Soybeans, Wheat-Soybeans (double cropped), rd.l. Conventional seed bed preparation	Beans, 30 bu. Beans, follow- ing Wheat, 25	
		bu. Wheat, 40 bu.	.400
57	Continuous Cotton. Residue shredded and left on soil surface until about April 1	Lint, 500 lbs.	<b>,</b> 430
58	Continuous Soybeans, rd.l. Conventional tillage	Beans, 30 bu.	.450
59		Lint, 600 lbs. Beans, 30 bu.	.450

Table No. 10 (Continued)

Order	Cropping System	Yields per Acre	Average Annual "C" Value
60	Continuous Cotton, rd.1. Effective cover crop every third year. Conventional tillage	Lint, 500 lbs.	
61	Continuous Corn, rd.l. Conventional tillage	Corn, 50 bu.	.460
62	Cotton-winter cover, Cotton, Soy- beans, Soybeans. Conventional tillage	Lint, 500 lbs. Beans, 25 bu.	.460
63	Continuous Soybeans, rd.l. Conventional tillage	Beans, 25 bu.	.500
64	Continuous Cotton, rd.1. Conventional tillage	Lint, 500 lbs.	<b>.</b> 500
65	Cotton, Soybeans, Soybeans, rd.1. Conventional tillage	Lint, 500 lbs. Beans, 25 bu.	.500
66	Continuous Cotton, rd.1. Conventional tillage	Lint, 450 lbs.	.550
67	Continuous Cotton, rd.1. Conventional tillage	Lint, 400 lbs.	.580
68	Continuous Corn for silage. Conventional tillage	Silage, 15 ton	.580
<b>6</b> 9	Continuous Soybeans, rd.1.	Beans, 15 bu.	.580
70	Continuous fallow. (No cover. Example: bare disturbed area.)		1.00

"C" Values for Pasture, Rangeland, and Idle Land  $\underline{1}/$  Also Woodland Grazed, Burned, or Recently Harvested  $\underline{5}/$ 

Table 11

Vegetal Canopy			Cov	er Th	at Cor	tacts	The S	urface
Type and Height of Raised Canopy 2/	Canopy Cover <u>3</u> /	Type <u>4</u> /		ent c	f Pere		Groun	d Cover
	(Percent)	·	0	20	40	60	80	95-100
Mo annucatable agranu				00	10	040	010	000
No appreciable canopy		G	.45	. 20	.10	.042	.013	
of tall weeds or brush		W	.45	.24	. 1.5	.090	.043	.011
Canopy of tall weeds	25	G	. 36	.17	.09	.038	.012	.003
or short brush		W	.36	.20	.13	.082	.041	.011
(0.5 m fall ht.)	50	Ĝ	.26	.13	.07	.035	.012	.003
(20 in. fall ht.)		w	. 26	.16	.11	.075	.039	.011
·	75	Ğ	.17	.10	.06	.031	.011	.003
		W	.17	.12	.09	,067	.038	.011
Appreciable brush	25	G	. 40	.18	.09	.040	.013	.003
or bushes		W	. 40	. 22	.14	.085	.042	.011
(2 m fall ht.)	50	Ĝ	. 34	.16	.085	.038	.012	.003
(6.5 ft. fall ht.)		W	. 34	. 19	.13	.081	.041	.011
•	75	Ğ	. 28	.14	.08	.036	.012	.003
		W	. 28	. 17	.12	.077	.040	.011
Trees but no appre-	25	G	.42	.19	.10	.041	.013	.003
ciable low brush		W	. 42	.23	.14	.087	.042	.011
(4 m fall ht.)	50	Ğ	.39	. 1.8	.01	.040	.013	,003
(13 ft. fall ht.)	<del></del>	W	.39	.21	.14	.085	.042	.011
	75	G G	.36	.17	.09	,039	.012	.003
	• ••	w	.36	.20	.13	.083	.041	.011

<sup>1/</sup> These values apply to "native pastures," to long uncropped cropland, and to similar lands having a herbaceous cover that is usually of low quality and which often includes brush or trees. The soil profile is relatively undisturbed, and plant roots proliferate in the surface layer. All values assume random but not necessarily uniform distribution of vegetation and mulch of appreciable depth where mulch exists. Lands devoid of cover and not a part of a cropping system have a C value of 1.00.

<sup>2/</sup> Average fall height of waterdrops from canopy to soil surface: m = meters,
 in. - inches, ft. = feet.

<sup>3/</sup> Portion of total-area surface that would be hidden from view by canopy in a vertical projection, (a bird's-eye view).

<sup>4/</sup> G: Cover at surface is green, grasslike plants, decaying compacted duff, or literal. W: Cover at surface is mostly broadleaf, herbaceous plants (as weeds) with little lateral-root network near the surface, and/or undecayed residue.

<sup>5/</sup> Multipy value by 0.7 for woodland grazed, burned or recently harvested.

6/ TABLE 12—Factor C for undisturbed forest land

Percent of area covered by concepy of trees and undergrowth	Percent of area covered by duff	Factor C?
100 7 5	100 90	0001001
70-45	85-75	002-004
40-20	70-40	.003009

<sup>&</sup>lt;sup>1</sup>Where effective litter cover is less than 40 percent or canopy cover is less than 20 percent, use table 11. Also use table 11 where woodlands are being grazed, harvested, or burned.

6/TABLE 12A.—Factor C for mechanically prepared woodland sites

			Soi	cond	ition² i	and w	eed co	ver <sup>1</sup>	
Site preparation	Mulch cover <sup>1</sup>	Exce	Excellent		Good		ir	Poor	
	, (OTEL	NC	WC	NC	₩C	NC	WC	NC	WC
	Percent								
Disked, raked,									
or bedded <sup>t</sup>	None	0.52	0.20	0 72	0 27	0.85	0 32	0.94	0.36
	10	.33	.15	.46	.20	.54	.24	60	.20
	20	.24	.12	.34	.17	.40	.20	.44	.27
	40	.17	.11	23	.14	.27	.17	.30	19
	60	.11	.08	.15	-11	.18	.14	.20	.13
	80	.05	.04	.07	.06	.09	.08	.10	.09
Burned <sup>1</sup>	None	.25	.10	.26	.10	.31	.12	.45	.17
	10	.23	.10	.24	.10	.26	.11	.36	.10
	20	.19	.10	.19	.10	.21	.11	.27	.1.
	40	.14	.09	.14	.09	.15	.09	.17	.1
	60	.08	.06	.09	.07	.10	.08	.11	.0
	80	.04	.04	.05	.04	.05	.04	.06	.0.
Drum chopped	<sup>3</sup> None	.16	.07	.17	.07	.20	.08	.29	.1
	10	.15	.07	.16	.07	.17	.08	.23	.1
	20	.12	.06	.12	.06	.14	.07	.18	.0
	40	.09	.06	.09	.06	.10	.06	.11	.0.
	60	.06	.05	.06	.05	.07	.05	.07	.0.
	80	.03	.03	.03	.03	.03	.03	.04	0

Percentage of surface covered by residue in contact with the

Good—Moderately stable soil aggregates in topsoil or highly stable aggregates in subsoil (topsoil removed during raking), only traces of litter mixed in.

Fair—Highly unstable soil aggregates in topsoil or moderately stable aggregates in subsoil, no litter mixed in.

Poor—No topsoil, highly eradible soil aggregates in subsoil, so litter mixed in.

3 NC-No live vegetation.

WC-75 percent cover of grass and weeds having an average drop fall height of 20 in. For intermediate percentages of cover, interpolate between columns.

\*Modify the listed C values as follows to account for effects of surface roughness and aging:

First year after treatment: multiply listed C values by 0.40 for rough surface (depressions >6 in); by 0.65 for maderalely rough; and by 0.90 for smooth (depressions <2 in).

For 1 to 4 years after treatments multiply listed factors by 0.7. For 44- to 8 years; use table 11-

More than 8 years: use table 7.

For first 3 years: use C values as listed.

For 3+ to 8 years after treatment: use table 11.

More than 8 years after treatment; use table 7.

6/ For complete discussion of C factors related to woodland, see page 32, 33, and 34 of Agri. HB 537.

Table 13
"C" Factors for Annual Cover, and Various Quantities of Mulch

Cover or Mulch	"C" Factor
Bare areas	1.00
🔒 ton straw mulch	.52
½ ton straw mulch	•35
3/4 ton straw mulch	<b>.</b> 24
l ton straw mulch	18
1을 ton straw mulch	.10
2 ton straw mulch	•06
3 ton straw mulch	.03
4 ton straw mulch	.02
Annual cover	.15

The ranges in listed C values are caused by the ranges in the specified forest litter and canopy covers and by variations in effective canopy heights. For mechanically prepared sites use table 12A.

<sup>&</sup>lt;sup>2</sup> Excellent soil condition—Highly stable soil aggregates in top-soil with fine tree roots and litter mixed in.

Table 14 "P" Practice Factor Values

Slope %	Up and Down Hill	Contour Farming	Contour Striperopping
.5 to 2	1.0	.60	.45
2.1 to 7	1.0	•50	•37
7.1 to 12	1.0	.60	.45

Slope-Leng	gth Limits for Contouring
Slope %	Maximum Slope Length
.5 to 2	400 feet
4 to 6	300 feet
8	200 feet
10	100 feet

Slope length may be increased 25 percent if residue cover after planting will regularly exceed 50 percent.

KRLSP TABLES

2000-	7.50 9.00 11.62 18.37	49.50 89.62 112.50 166.12 229.50 302.62 475.87	2000•	8.50 10.20 13.17 20.82 29.75 56.10 101.57 127.50 188.27 260.09 342.97 539.32
1600-	7.12 8.25 10.87 17.25	425.62 40.25 80.25 100.87 148.50 205.12 425.62	1600.	8.07 9.35 12.32 19.55 28.05 51.42 90.95 114.32 168.29 232.47
HILL 1200.	6.37 7.50 10.12 15.75	23.00 69.37 87.37 128.62 177.75 234.37	N HILL 1200.	7.22 8.50 11.47 17.85 25.50 45.90 78.62 99.02 145.77 201.45
UP AND DOWN HILL 800. 120	5.62 6.75 9.00 13.87	19.07 34.12 56.62 71.25 105.00 145.12 191.24	UP AND DOWN HILL 800. 1200	6.37 7.65 10.20 15.72 22.52 38.67 64.17 80.75 119.00 164.47 216.75
•009	5-25 6-00 8-25 12-75	16.51 49.12 61.50 90.75 125.62 165.74 260.62	•009	5.95 6.80 9.35 14.45 20.82 34.42 55.67 69.70 102.85 142.37 187.84
0.15	4.50 5.25 7.12 11.25	16.12 25.87 40.12 50.25 74.25 102.37 135.00	ABLES 0.17 400.	5.10 5.95 8.07 12.75 18.27 29.32 45.47 56.95 84.15 116.02 153.00
K= 0 300.	4.12 4.87 6.75 10.12	14.82 23.25 34.50 43.50 64.12 88.87 117.00	KRLSP TABLES  K= 0.17  300.	4.67 5.52 7.65 11.47 16.57 26.35 39.10 49.30 72.67 100.72 132.60
200-	3.75 4.50 5.62 9.00	15.12 19.50 28.12 35.62 52.50 72.37 95.62	200•	4.25 5.10 6.37 10.20 14.87 22.10 31.87 40.37 59.50 82.02 108.37
R= 250.	8.97 9.97 0.27	10.50 15.00 19.87 25.12 37.12 51.00 67.50	R= 250. 100.	3.40 3.82 5.10 8.50 11.00 17.00 22.52 28.47 42.07 76.50
50.	2-25 3-60 3-75	8.62 11.25 13.87 17.62 26.25 36.00 47.62	\$0 <b>.</b>	2.55 3.40 4.25 6.80 9.17 12.75 15.72 19.97 29.75 40.80 53.97
<b></b>		3.00 5.00 6.00 10.00 12.00 16.00	PERCENT SLOPE	0.25 0.50 1.00 2.00 3.00 4.00 6.00 8.00 10.00

	2000-	10.00	12.00	15.50	24.50	35.00	99	119,50	150,00	221.50	306.00	403.50	626 40	034.49			2000-		12.00	14.40	24.41	29 40	42.00	79.20	143.40	000	00 00 00 00 00 00 00 00 00 00 00 00 00	267 10	701-17	761.39
	1600.	9.50	11.00	14.50	23.00	33.00	60.50	107.00	134.50	198.00	273.49	360-49	267 40	•			1600		11.40	13.20	17.40	27-60	39-60	72.60	128.40	161.39	24.460	200 000	61.026	680,99
HILL	1200.	8.50	10.00	13.50	21.00	30.00	54.00	92.50	116.50	171.50	237.00	312.50	491 50	1					10.20	12.00	16.20	25.20	36.00	64.80	111.00	139.80	205-80	284.20	375.00	589.79
UP AND DOWN HILL	*00°	7.50	9.00	12.00	18.50	26.50	45.50	75.50	95.00	140.00	193.50	255.00	401.49	5		NACO ONA GIT			00-6	10.80	14.40	22.20	31.80	54.60	90.60	114.00	168.00	232-20	305.99	481.79
	•009	7.00	8.00	11.00	17.00	24.50	40.50	65.50	82,00	121.00	167.50	220.99	347.50	200			•009		8.40	09*6	13.20	20.40	29.40	48.60	78.60	98,40	145.20	201.09	265-19	417.00
0*50	<b>4</b> 00 <b>*</b>	9.00	7.00	9.50	15.00	21.50	34.50	53,50	67.00	99.00	136.50	180,00	783.43	• •	3LES	0-24	400		7.20	8.40	11.40	18.00	25.80	41.40	64.20	80.40	118.80	163.79	216.00	340.19
	300°	5.50	6.50	9.00	13.50	13.50	31.00	46.00	58.00	85.50	118.50	156.00	245.50	•	KRLSP TABLES		300		9-90	7.80	10.80	16.20	23.40	37,70	54-20	09*69	102.60	142.20	187.20	294-59
	200•	5.00	00-9	7.50	12.00	17.50	26.00	37.50	47.50	70.00	96.50	127.50	200.50				200		9-00	7.20	9-00	14.40	21.00	31.20	45.00	57.00	84.00	115.80	153.00	240.59
R= 250.	100.	4-00	4-50	9.00	10.00	14.00	20.00	26.50	33.50	49.50	68.00	00.06	141,50	•		R= 250.	100.		4.80	5.40	7.20	12.00	16.80	24.00	31.80	40.20	59.40	81.60	08.0	169.80
	<b>20</b> •	3.00	4.00	5.00	8.00	11.50	15.00	18.50	23.50	35.00	48.00	63.50	100.00				<b>20.</b>		3.60	4-80	60.9	09.6	13.30	18.00	22.20	28.20	45.00	57.60	76-20	120-00
	PERCENT SLOPE	0.25	0.50	1.00	2*00	3-00	4.00	5.00	9.00	8.00	10.00	12.00	16.00	9			PERCENT	SLUFE	0.25	0.50	1.00	2.00	3,00	4.00	2°-4	00*9	8.00	10-00	12-00	16.00

KRLSP TABLES

6	2000	14.00	16.80	21.70	34.30	49.00	95.40	167.30	210.00	310.09	428-39	564-89	888.29				2000	16.00	19.20	24.80	39-20	56.00	105.60	191.20	240.00	354.39	489.59	642.59	1015.19
	1600.	13,30	15.40	20.30	32.20	46.20	84.70	149.80	188-29	277.19	382.89	504.69	4.49				1600.	15.20	17.60	23.20	36.80	52.80	96.80	171.20	215.19	316.79	437.59	576.79	907.99
I	1200.	11.90	14.00	18.90	29.40	45.00	75.60	129.50	163.10	240-10	331.79	437.50	688.09			N HILL	1200.	13.60	16.00	21.60	33.60	48.00	86.40	148.00	186.40	274.40	379.20	500.00	786.39
UP AND DOWN	<b>.</b> 008	10.50	12.60	16.80	25.90	37.10	63.70	105.70	133.00	196.00	270.89	356.99	- 1			UP AND DOWN HILL	800.	12.00	14.40	19.20	29.60	45.40	72.80	120.80	152.00	224.00	309.59	407.99	642.39
	.009	9.80	11.20	15.40	23,80	34.30	56.70	91.70	114.80	169,39	234.50	309,39	646.49				•009	11.20	12,80	17.60	27.20	39.20	64.80	104.80	131.20	193.60	8.0	ð	•
0.28	400*	8-40	9.80	13,30	21-00	30.10	48.30	74.90	93.80	138.60	191.09	252.00	305 80	3	BLES	0.32	400*	09*6	11,20	15.20	24.00	34.40	55.20	85.60	107.20	158,40	218.39	288.00	453.59
	300.	7.70	~~	12.60	18.93	27.30	43.40	64.40	81.20	119.70	165,89	218,39	272 40	•	KRLSP TABLES	K= 0	300•	8.80	10.40	14.40	21.60	31.20	49.60	73.60	92.80	136.80	189.60	249.60	392.79
	200-	7.00	8 40	10.50	16.80	24.50	36.40	52.50	66.50	98.00	135.10	178.50	200 40	0.00			200-	8,00	09.6	12,00	19.20	28.00	41.60	00.09	76.00	112.00	154.40	204.00	320.79
R= 250.	100.	5.60	6.30	8.40	14.00	19.60	28.00	37.10	46.90	69.30	95.70	126.00	0.000	01.041		R= 250.	100.	6.40	7.20	09*6	16.00	22.40	32.00	45.40	53.60	79.20	108.80	144.00	226.40
	÷05	4-20	5.60	2007	11.20	16.10	21.00	25.90	32.90	49.00	67.23	06.88		•			50.	4.80	6.40	8.00	12.80	18.40	24-00	29.60	37.60	56.00	76.80	101.60	160.00
	PERCENT SLOPE	26.05		00,	2-00	60.4	4.00	00.4	00-9	8.00	00-01	12.00	) (	16•00			PERCENT SLOPE	0.25	0.50	1.00	2.00	3-00	4.00	5.00	00.9	00-9	10.00	12.00	16.00

PEKCENT	50.	R= 250. 100.	200-	K = 0 300*	6.37	, 603.	UP AND DOWN 800.	N HILL 1200.	1600.	2000*
	5-55	7.40	9.25	10.17	11-10	12.95	13.87	15.72	17.57	18.50
	7.40	8,32	11-10	12.02	12,95	14.80	16.65	18.50	20.35	22.20
	9.25	11.10	13.87	16.65	17.57	20,35	22.20	24.97	26.82	28.67
	14.80	18.50	22.20	24.97	27.75	31.45	34-22	38.85	42.55	45.32
	21.27	25.90	32.37	36.07	39.77	45.32	49.02	55.50	61.05	64.75
	27.75	37.00	48.10	57.35	63.82	74.92	84.17	06*66	111.92	122.10
	34.22	49.02	69.37	85.10	98.97	121.17	139.67	171.12	197.94	221.07
	43.47	61.97	87.87	167.30	23.	151.70	175.75	.215.52	248.82	277.50
	64.75	91.57	129.50	158.17	83.	223.84	258.99	317.27	366.29	409.17
	88.50	25	178.52	219.22	52.	309.87	357.97	438.44	505.97	566.09
	117.47	166.50	235.87	288.59	332.99	408-84	471.74	578.12	666.92	746.47
	· (		000000000000000000000000000000000000000	V - 707				) (	) (	
	0	Į D	26.010	- I • + C +	• * V	Ç.	74	77*606	1044.81	1115-82
				KRLSP TABLES	BLES					
		R=, 250.			0.43		UP AND DOWN	N HILL		
ERCENT LOPE	50.	100	2002	300.	400*	<b>•</b> 009	800.	1200.	1600.	2000.
	6.45	8.60	10.75	11.82	12.90	15.05	16.12	18.27	20.42	21.50
	8.60	19.6	12.90	13.97	15.05	17.20	19,35	21.50	23.65	25.80
1.00	10.75	12.90	16.12	19.35	20-42	23.65	25.80	29.02	31.17	33.32
	17.20	21.50	25.80	29.02	32.25	36.55	59.77	45.15	49.45	52-67
	24.72	30.10	37-62	41.92	45.22	52.67	26.95	64.50	70.95	75.75
	32-25	43.00	55.90	66.65	74-17	87.07	97.82	116.10	130.07	141.90
	39.77	56.97	80.62	98.90	115.02	140.82	162.32	198.87	230.04	256.92
	20.52	72.02	102.12	124.70	144.05	176-29	204.25	250.47	289.17	322 +50
	75,25	106.42	150.50	183.82	212.84	260.14	300.99	368.72	425.69	476-22
	103.20	146,20	207.47	254.77	293.47	360.12	416.02	509.54	588-02	657.89
	136.52	193.50	274.12	335.39	386.99	475-14	548-24	671.87	775.07	867.52
	215.00	304-22	431-07	527.82	609-52	7.1	863.22	1056.72	1220-12	1364.17

		R= 250.			0,49		UP AND DOWN HILL	4 HILL		
PERCENT SLOPE	\$0 <b>.</b>	100*	200-	300	400*	•009	8008	1200-	1600.	2000-
0.25	7.35	9.80	12-25	13,47	14-70	17.15	18.37	20.82	23-27	24.50
0.50	9.80	11-02	14.70	15.92	17-15	19.60	22.05	24.50	26.95	29.40
1.00	12.25	14.70	18.37	22.05	23.27	26.95	29.40	33.07	35.52	37.97
2.00	19.60	24.50	29.40	33.07	36+75	41.65	45.32	51.45	56.35	70.09
3.00	28-17	34.30	42.87	47.17	52.67	60-02	64.92	73.50	80.85	85.75
4.00	36.75	49.00	63.70	75.95	84.52	99.22	1111.47	132,30	148.22	161.70
5.00	45.32	64.92	91.87	112.70	131.07	160.47	184.97	226.62	262.14	292,77
00.9	57.57	82.07	116.37	142-10	164.14	200.89	232.75	285.42	329.52	367.50
8.00	85.75	121.27	171.50	209.47	242.54	296.44	342.99	420.17	485.09	542.67
10-00	117.60	166.60	236-42	290.32	334.42	410.37	474-07	580.64	670.07	249-64
12,00	155.57	220.50	312.37	382.19	440.99	541.44	624-74	765-62	883.22	988.57
100		27776	· · · · · · · · · · · · · · · · · · ·	77 107	207	051 27			1000	- 1
10.00	242•00	240.01	77-164	007-46	074.31	851-36	985.01	1504*1	1590*31	1554.52
				KRLSP TABLES	BLES					
		R= 250.		. Κ 0 = Χ	0.55		UP AND DOWN HILL	N HILL		
PERCENT SLOPE	50.	100-	2002	300•	4004	•009	800•	1200.	1600.	2000-
0.25	8.25	11.00	13.75	15.12	16.50	19.25	20.62	23,37	26.12	27.50
0.50	11.00	12.37	16.50	17.87	19.25	22.00	24.75	27.50	30.25	33.00
1.00	13.75	16.50	20.62	24.75	26.12	30.25	33.00	37.12	39.87	42.62
2.00	22.00	27.50	33.00	37.12	41.25	46.75	50.87	57.75	63.25	67.37
3.00	31.62	38.50	48.12	53.62	59.12	67.37	72.87	82.50	90.75	96.25
4.00	41.25	55.00	71.50	85.25	94.87	111.37	125.12	148.50	166.37	181.50
5.00	50.87	72.87	103.12	126.50	147.12	180.12	207.62	254.37	294.25	328.62
00*9	64.62	92.12	130,62	159.50	184.25	225.50	261.25	320.37	369.87	412.50
8*00	96.25	136.12	192,50	235.12	272.24	332.74	384.99	471-62	544.49	609-12
10.00	132.00	187.00	265.37	325.87	375.37	460.62	532-12	651.74	752.12	841.49
12,00	174.62	247.50	350.62	428.99	464.99	0	701.24	859.37	991.37	1109.62
16.00	275.00	389-12	551.37	675.12	779-62	955-62	1104-12	1351.62	1560.62	1744.87

	2000	8.75	06*6	12.78	20.21	28.87	54.45	98.58	123.75	182.73	252-44	332.88	523.46			2000-	2	700	77-11	22 00	32,72	61.71	111-73	140.25	207.10	286-10	377.27	593.25
	1600.	7.83	6.07	11.96	18.97	27.22	49.91	88.27	110.96	163.34	225.63	297.41	468-18			1600.	a a	0.00	10.20	01.10	30.85	56-56	100-04	125.75	185,13	255.72	337.06	530-61
HILL	1200-	7.01	8.25	11.13	17.32	24.75	44.55	76.31	96.11	141.48	195.52	257.81	405.48		=======================================		σ	, ,	,	9.6	28.05	7 0	6.4	08.9	m	21.5	92.1	59.5
UP AND DOWN HILL	800°	6.18	7.42	06*6	15.26	21.86	37.53	62.28	78.37	115,50	159.63	210.37	331.23		UP AND DOWN		7.01	7 8	11.22	17.29	24.77	42.54	70.59	88-82	130.90	180.92	238.42	375.40
	•009	5.77	09*9	4.07	14.02	20.21	33.41	54.03	67.65	99.82	138.18	w	286.68			<b>•</b> 009	6.54	7.48	10.28	15.89	22.90	37.86	61.24	76.67	113.13	156.61	206-63	324.91
0.15	400*	4.95	5.77	7.83	12,37	17.73	28.46	44.13	55.27	81.67	112.61	148.50	233,88	3L ES	0.17	400*	5.61	6.54	. 60	14.02	20.10	32,25	50.02				68.30	
K = 0.	300•	4.53	5.36	7.42	11.13	16.08	25.57	37.95	47.85	70.53	97.76	128.70	202.53	KRLSP TABLES	11	300.	5.14	6.07	8.41	12.62	18.23	28.98	43.01	54.23	46.62	10.	145.86	Ŕ.
	200.	4.12	4.95	6.18	06*6	14.43	21.45	30,93	39.18	57.75	79.61	105.18	165.41			200-	4.67	5.61	7.01	11.22	16.36	24.31	35.06	14-44	65.45	90.22	119-51	167-46
R= 275.	100T	3,30	3.71	4.65	8.25	11.55	16.50	21.86	27.63	40.83	56.10	74.25	116.73		R= 275.	100.	3.74	4.20	5.61	9.35	13.09	18.70	24.77	31.32	46.28	63.58	84.15	132,30
	50.	2.47	3.30	4.12	09*9	9*48	12-37	15.26	19.38	28.87	39.60	52.38	82.50			• 05	2.80	3.74	4.67	7-48	10.75	14.02	17.29	21.97	32-72	44.88	59.37	93.50
	PERCENT SLOPE	0.25	0.50	1.00	2.00	3.00	4*00	2.00	00*9	8.00	10.00	12.00	16.00			PERCENT SLOPE	0.25	0.50	1.00	2.00	3.00	4.00	2.00	9.00	8-00	10.00	12.00	10.01

KRLSP TABLES

2000.	11.00 13.20 17.05 26.95 38.50 72.60 131.45 165.00 243.64 336.59		2000*	13.20	32-34	87.				532.61 837.53
1600-	10.45 12.10 15.95 25.30 36.30 66.55 117.70 147.95 217.79 390.84 396.54		1600.	12.54						
HILL 1200.	9.35 11.00 14.85 23.10 33.00 59.40 101.75 128.65 260.70 343.75		1 HILL 1200.	11.22	27.72	71.28	122.10	226.38	312.83	412.50 648.77
UP ANČ DÖWN 800.	8.25 9.90 13.20 20.35 20.35 50.05 83.05 104.50 212.85 280.50 441.64		UP AND DOWN 800.	9.90	24.42	* 0	oυr	$\sim$	. v	OΦ
•009	7.70 8.80 112.10 118.70 26.95 44.55 72.05 90.20 133.10 184.25 243.09		•009	9.24	22.44	•	86.4	08°2 59.7	21.1	291.71 458.69
0.20	6.60 10.45 10.45 16.50 23.65 37.85 73.85 73.85 108.90 150.14 198.00	BLES	0.24	7.92	19.80	ė in	<u></u>	888	80.	<b>⊬.</b> 4
K= 0.	6.05 7.15 9.90 14.85 24.10 50.60 63.83 171.60	KRLSP TABLES	K= 0. 300.	7.26	17.82	40.92	60.72	76.56 112.86	156.42	205.92 324.05
200-	5.50 6.60 8.25 13.20 19.25 28.60 41.25 77.00 106.15 140.25		200-	7.92	15.84	34.32	49.50	62.70	127,38	168,29
R= 275. 100.	4.40 4.95 6.60 11.00 15.40 22.00 29.15 36.85 36.85 74.80 99.00		R= 275. 100.	5.28	M ∶	φα	4	ላ ሆ	יסיר	118.80
50.	2.30 6.40 11.00 11		50•	3.96		7.6 9.8	4.4	1.0 2.0	. M	a) 🗘
	0.50 0.50 0.50 1.00 2.00 5.00 10.90 12.90 16.00		PERCENT SLUPE	6.25 0.50	2.00	4.00 4.00	5.00	٠ د د د د	10.03	12.00 16.00

2000	15.40 18.48 23.87 37.73 37.73 53.90 101.64 184.02 231.00 341.10 471.23 621.38		2000•	17.60 21.12 27.28 43.12 61.60 116.16 210.32 264.00 369.81 538.55
1600	14.63 16.94 22.33 35.42 50.82 93.17 164.77 207.12 304.91 421.18 555.16		1600.	16-72 19-36 25-52 40-48 58-08 106-48 188-32 236-72 348-47 481-35
IN HILL 1200.	13.09 15.40 20.79 32.34 46.20 83.16 179.41 264.10 364.97 481.25		1 HILL 1200.	14.96 17.60 23.76 36.96 52.80 95.04 162.80 205.04 301.83 417.11 550.00
UP AND DOWN HILL 800. 120	11.55 13.86 18.48 28.49 40.81 70.07 116.27 146.30 215.59 297.98 392.69		UP AND DOWN HILL 800. I200.	13.20 15.84 21.12 32.56 46.64 80.08 132.88 167.20 246.39 340.55 448.79
•009	10.78 12.32 16.94 26.18 37.73 62.37 100.87 126.28 186.33 257.95		•009	12.32 14.08 19.36 29.92 43.12 71.28 115.28 144.32 212.95 212.95
0.28	9.24 10.78 14.63 23.10 33.11 53.13 82.39 103.18 152.45 277.20 436.58	BLES	400*	10.56 12.32 16.72 26.40 37.84 60.72 94.16 117.24 240.23 316.79
300.	8.47 10.01 13.86 20.79 30.03 47.74 70.84 89.82 131.67 182.49 240.23	KRLSP TABLES	K= 0 300.	9.68 15.44 15.84 23.76 34.32 54.56 102.08 150.48 274.55 432.08
200•	7.70 9.24 11.55 18.48 26.95 40.04 57.75 13.15 107.80 148.61 196.35		200-	8.80 10.56 13.20 21.12 30.80 45.76 66.00 83.60 123.20 169.84 224.39
R= 275. 100.	6.16 6.93 9.24 15.40 21.56 30.80 40.81 76.23 104.72 138.60		R= 275. 100.	7.04 7.92 10.56 17.60 24.64 35.20 46.64 58.96 87.12 119.68 158.40
5C.	4.62 6.16 7.10 12.32 17.32 17.33 18.49 36.19 53.90 73.92 97.79			5.28 7.04 8.80 14.08 20.24 26.24 32.56 41.36 61.60 84.48 111.76
PERCENT SLOPE	0.25 0.25 0.50 1.00 2.00 3.00 4.00 5.00 6.00 10.00 12.00 16.00		PERCENT SLOPE	0.25 0.50 1.00 2.00 2.00 4.00 4.00 1.00 1.00 1.00 1.00 1.00 1

KRLSP TABLES

2000*	20.35 24.42 31.54 49.85 71.22 134.30 243.18 305.25 450.75 622.70 821.12		2000-	23.65 28.38 36.65 57.94 82.77 156.08 282.61 354.75 523.84 723.68 954.27
1600.	19.33 22.38 29.50 46.80 67.15 123.11 217.74 273.70 402.92 556.57 733.61		1600.	22.46 26.01 34.29 54.39 78.04 143.08 253.05 318.09 468.26 646.82 852.58
1 HÍLL 1200.	17.29 20.35 27.47 42.73 61.05 109.89 188.23 237.07 349.00 482.29 635.93		1200.	20.10 23.65 31.92 49.66 70.95 127.71 218.76 275.52 405.59 560.50 739.06
UP AND DOWN HÍLL 800. 120	15.26 18.31 24.42 37.64 53.92 92.59 153.64 193.32 284.89 393.77 518.92		UP AND DOWN HILL 800. 120	17.73 21.28 28.38 43.75 62.67 107.60 178.55 224.67 331.09 457.62 603.07
•009	14.24 16.28 22.38 34.59 49.85 82.41 133.29 166.86 246.23 340.86 449.73		•009	16.55 18.92 26.01 40.20 57.94 95.78 154.90 193.92 286.16 396.13 522.66
0.37	12.21 14.24 19.33 30.52 43.75 70.20 108.87 136.34 201.46 277.77 366.29 576.92	BL ES	0.43	14.19 16.55 22.46 35.47 50.84 81.59 126.52 158.45 234.13 322.82 425.69 670.47
K= 0. 300.	11.19 13.22 18.31 27.47 39.68 63.08 93.61 118.03 173.99 241.14 317.45	KRLSP TABLES	K= 0 300.	13.00 15.37 21.28 31.92 46.11 73.31 108.79 137.17 202.20 280.25 368.93
200-	10.17 12.21 15.26 24.42 24.42 35.61 76.31 76.31 142.45 196.37 259.46		200.	1182 14.19 17.73 28.38 41.38 61.49 88.68 112.33 165.54 228.22 301.53
R= 275. 100.	8.14 9.15 12.21 20.35 28.49 40.70 53.92 68.17 100.73 138.38 183.14		R= 275. 100.	9.46 10.64 14.19 23.65 33.11 47.30 62.67 79.22 117.06 160.82 212.85
50.	6.10 8.14 10.17 16.28 23.40 30.52 37.64 47.82 71.22 97.68		50.	7.09 9.46 11.82 18.92 27.19 35.47 43.75 55.57 82.77 113.52 150.17
PERCENT SLOPE	0.25 1.00 1.00 2.00 3.00 4.00 4.00 12.00 16.00		PERCENT SLUPE	0.25 0.55 0.50 2.00 2.00 4.00 6.00 12.00 16.00

	<b>2</b> 000.	26.95	32.34	41.77	66.02	94.32	177.86	322.05	404-25	596.94	824.66	1087.43	1709.97				2000-	30 -25	36.30	46-88	74.11	105.87	199.64	361.48	453.75	670.03	925.64	1220.58	1919*36
	1600.	25.60	29.64	39.07	61-98	88.93	163.04	288.36	362-47	533.60	737.08	971.54	4				1600.	28.73	33.27	43.86	69.57	99.82	183.01	323.67	406.86	598.94	827,33	1040,51	1716.68
N HILL	1200.	22.90	26.95	36.38	56.59	80.85	145.52	249.28	313.96	462.19	638.71	342.18	1324_59	) ) )		N HILL	1200.	25.71	30.25	40-83	63.52	90.75	163,35	279.81	352.41	518.78	716.92	945.31	1486.78
UP AND DOWN HILL	300°	20.21	24.25	32.34	49.85	71.41	122.62	203.47	256.02	377.29	521.48	7	1082.04	•		UP AND DOWN HILL	800.	22.68	27.22	36.30	95,96	80-16	137.63	228-38	287.37	423-49	585.33	771.37	1214-53
	•009	18.86	21.56	29.64	45.81	66.02	109.14	176.52	220.98	326.09	451.41	595,59	936.51	) ) )			•009	21.17	24.20	33.27	51.42	74-11	122.51	198-13	248.04	366.02	506.68	668.52	1051-18
67*0	<b>4</b> 00 <b>4</b>	16.17	18.86	25.60	40.42	57.94	92.97	144.18	180.56	266.80	367.86	485.09	764.03	)	BLES	0.55	400*	18.15	21.17	28-73	45.37	65.03	104.36	161.83	202.67	299.47	412.91	44.4	857.58
\ \ \ \	300.	14.82	17.51	24.25	36.38	52-55	83.54	123.97	156.30	230.42	319,35	420.41	661-62	1 2 4 3)	KALSP TABLES	Κ= 0	300.	16.63	19.66	27-22	40.83	58.98	93.77	139.15	175.44	258.63	358.46	471-89	142.63
	200.	13.47	16.17	20.21	32,34	47.16	70.07	101.06	128.61	183.64	260.06	343.61	540.24	-			200.	15.12	18.15	22.68	36.30	55.93	18.65	113,43	143.68	211.75	291.91	385.68	15.909
R= 275.	100.	10.78	12.12	16.17	26.95	37.73	53.90	71.41	90.25	133.40	183.26	242.54	281.34	- • •		R= 275.	100.	12.10	13.61	14.15	30.25	42.35	60.50	80.16	101.33	149.73	205.70	272.25	428.03
	¥0.	8.08	10.78	13.47	21.56	30.99	40.42	49.85	63,33	94.32	, .	-	1 4	•			÷09	9.07	12.10	15.12	24.20	34.78	45.37	55.96	71.CE	105.87	145.20	192.68	302.50
	PERCENT SLOPE	0.25	0.50	1.00	2.00	3,00	4.00	5.00	90.00	8-00	10.00	12.00	71				PERCENT SLOPE	0.25	0.50	1.00	7.00	3.00	4.00	2.00	00-9	8 <b>.</b> 00	10.00	12.00	Ç

	<b>.</b> 0005	9.00	10.80	13.95	22.05	31.50	59.40	107.55	135.00	199.34	275.39	363.14	27, 07	50.T16			2000	10.20	12.24	, p.	70 07	CC - +7	35.70	67.32	121.89	153.00	225.92	312.11	411.56	647.18
	1600.	8.55	06*6	13.05	20-70	29.70	54.45	96-30	121.05	178.19	246.14	324.44	10 77	210.14			1600.	69*6	11.22	100	,	72.40	33.66	61.71	109.14	137-19	201.95	278.96	367.70	578.84
HILL	1200.	7.65	00-6	12-15	18.90	27.00	48.60	83_25	104,85	154,35	213,29	281.25	71.677	447*74		HILL	1260.	8.67	10.20	1 0	13.11	74.17	30.60	55.08	94.35	118-83	174.93	241.73	318.75	501.32
4	800.	6.75	8.10	10.80	16.65	23.85	40.95	67.95	85.50	126-00	174-14	229.49	7	361.34		UP AND DOWN HILL	800.	7.65	30	7	52°71	18.81	27.03	46.41	77.01	06*96	142.80	197.37	560.092	409.52
UP	<b>.</b> 009	6-30	7.20	06*6	15,30	22.05	36,45	58.95	73.80	108,90	150.75	198-89	100	312.14		J	•009	7.14	2 L a	01.	11.22	17.34	24.99	41.31	66.81	83.64	123.42	170.85	225-41	354.44
0.15	<b>+</b> 00 <b>+</b>	5.40	6.30	8.55	13,50	19,35	31.05	48.15	60.30	89.10	122.85	162.00	704	255.14	ILES	0.17	<b>.</b> 00 <b>.</b>	6-12	7 7 7	+1 · ·	69.6	15,30	21.93	35-19	54.57	68.34	100.98	139-23	133.60	289-16
п	300-	4.95	5.85	8.10	12.15	17.55	27.90	41.40	52.20	76.95	106.65	440.39	0000	220.94	KRLSP TABLES	K= 0.	300.	5.61	22.7	0.00	₽. I.	13.77	19.89	31.62	46.92	59.16	87.21	120,87	53.1	50.4
	200-	4.50	7	6.75	10.80	15.75	23.40	33.75	42.75	63.00	86.85	114.75	7 - 4 - 7 - 7	180.44			200.	) I		71.0	7.65	12.24	17.85	26.52	38.25	48.45	71-40	98.43	130.05	204.50
R= 300*	100+	3.60	4.05	5.40	00°6	12.60	18.00	23.85	30.15	44.55	61.20	200	20.4	127.35		R= 300.	100-	4		4.04	6.12	10.20	14-28	20-40	27.03	34-17	50.49	69.36	91.80	144.33
	÷0.	2.70	3.60	4.50	7.20	3	13,50	6.5	-	• •		, . • • .	•	၀ ၀			÷0÷	20.00	) (	4.03	5.10	8.16	11.73	15.30	18.87	73.07	35.70	48-46	64.77	192,50
	PERCENT SLUPE	0.25	25.0	. 0.	2,06	3.00	50 - 5 0.04	, O.3	30. 4	000	000	0 0	72.40	16.00			PERCENT SLIDE	, , , , , , , , , , , , , , , , , , ,	£2•7.	00*3	1.00	2.00	3.00	4.00	00.4	50-9	× 20	35-01:	12.00	W)

2000.	12.00 14.40 18.60 29.40 42.00 79.20 143.40 180.00 265.79 367.20 484.19	2000. 14.40 17.28 22.32 35.28 50.40 95.04 172.08 216.00 318.95 440.63 581.03
1600.	11.40 13.20 17.40 27.60 39.60 72.60 128.40 161.39 237.60 328.19 432.59 680.99	13.68 13.68 15.84 20.88 33.12 47.52 87.12 154.68 193.67 285.11 393.83
N HILL 1200.	10.20 12.00 16.20 25.20 36.00 64.80 1111.00 139.80 205.80 284.39 375.00 589.79	HILL 1200. 12.24 14.40 19.44 30.24 43.20 77.76 133.20 167.76 246.95 341.27
UP AND DOWN HILL 800. 120	9.00 14.40 22.20 31.60 31.60 90.60 114.00 168.00 232.20 305.99 481.79	UP AND DOWN 800- 10-80- 17-96- 17-96- 17-28- 26-64- 38-16- 65-52- 108-72- 136-80- 278-64- 367-19- 578-15-
•009	8.40 9.60 13.20 20.40 29.40 48.60 78.60 98.40 145.20 201.00 265.19	600. 10.08 11.52 15.84 24.48 35.28 58.32 94.32 118.08 174.23 241.20 318.23
0.20	7.20 8.40 11.40 18.00 25.80 41.40 64.20 80.40 118.80 118.80 163.79 216.00 340.19	8.64 10.08 13.68 21.60 30.96 49.68 77.04 96.48 142.55 196.55 259.20
K= 0 300•	6.60 7.80 10.80 10.80 16.20 23.40 27.20 69.60 102.60 187.20 187.20 294.59 34	K= 0 300. 7.92 7.92 9.36 12.96 19.44 28.52 123.12 170.64 35.52
200•	6.00 7.20 9.00 14.40 21.00 31.20 45.00 57.00 115.80 115.80	200. 7.20 8.64 10.60 17.28 25.20 37.44 54.00 68.40 100.80 138.96 183.60
R= 300. 100.	4.80 5.40 7.20 12.00 16.80 24.00 31.80 40.20 59.40 81.60 108.00	R= 300- 100. 100. 5.76 6.48 8.64 14.40 20.16 28.80 38.16 48.24 71.28 97.92 129.60
50.	3.60 4.80 6.00 9.60 13.80 18.00 22.20 28.20 42.00 57.60 120.00	50. 4.32 5.76 7.20 11.52 16.56 21.60 26.64 33.84 50.40 69.12 91.44
PERCENT SLOPE	0.25 1.00 7.00 7.00 7.00 6.00 8.00 12.00	PERCENT SLUPE 0.25 0.25 1.00 2.00 2.00 6.00 6.00 12.00 16.00

KALSP TABLES

	2000-	16.80	20-16	26.04	41-16	58-80	110.88	200.76	252.00	372.11	514.07	677.87	1065.95			2000.	r	13.50	23.04	29.76	47.04	67.20	126.72	229.44	288.00	425.27	587.52	774-71	1218.23
	1600-	15.96	18.48	24.36	38.64	55.44	101.64	179.76	225.95	332.63	459.47	605.63	c			1600.		10-24	21-12	27.84	44-16	63.36	116.16	205.44	258,23	380.15	525.11	692.15	1089.59
I HILL	1200-	14.28	16.80	22.68	35.28	50.40	90.72	155.40	195.72	288.11	398.15	524.99	825.71			1200.	,,	7C*0T	19.20	25.92	40.32	57-60	103.68	177.60	223.68	329.27		00.009	943.67
UP ANG DOWN HILL	800-	12.60	15-12	20.16	31.08	44.52	76.44	126-84	159.60	235.19	325.07	428.39	674.51		0.00 G	800. 1200.	07 7.	O+ + +	17.28	23.04	35.52	50.88	87.36	144.96	182.40	268.79	371.52	489.59	770.87
	•009	11.76	13-44	18-48	28.56	41.16	68+04	110.04	137-76	203.27	281.39	371.27	583.79			•009	77 64	1	15.36	21.12	32.64	40-14	77.76	125.76	157.44	232.31	321.59	424-31	667-19
0.28	<b>*</b> 00 <b>*</b>	10.08	11.76	15.96	25-20	36.12	57.96	89.88	112,56	166.32	229.31	302,39	476-27	BLES	, ,	400	11	-	13.44	18.24	28.80	41-28	66-24	102.72	128.64	190.08	262.07	345.59	
K= 0,	300-	9-24	10-92	15-12	22.68	32.76	52.08	77.28	97.44	143.64	199.08	262.07	412.43	KRLSP TABLES	, ,		74	00.01	12.48	17.28	25.92	37-44	53.52	88.32	111.36	164.16	227.52	299.52	471+35
	200•	8.40	10.08	12.60	20.16	29.40	43-68	63.00	79.80	117.60	162.11	214.19	336.83			200-	0	7.00	11.52	14.40	23.04	33.60	49.92	72.00	91.20	134.40	185.27	244.79	384.95
R= 300.	1001	6.72	7.56	10+08	16-80	23.52	33+60	44.52	56-28	83.16	114-24	151,20	237.72		0	ł	7	00**	8.64	11.52	19,20	26.88	38.40	50.88	64,32	95.04	130.56	172.80	271.67
	50.	5-04	6-72	8.40	13.44	19.37	25.20	31.08	39.48	58.80	80.04	106.68	168.00			-04	7.	01*6	7.68	09*6	15,36	22.08	28.80	35-52	45,12	67.20	92.16	2	192.00
	Percent Slope	0.25	0.50	1.00	2.00	3.00	4*00	5.00	00-9	8.00	10.00	12-00	16-00			PERCENT	טיני טיני טיני	67*0	0.50	1.00	2.00	3.00	4.00	5.00	9.00	8.00	10.00	2	16.00

2000-		72.20	56-64	34.41	54.39	77.70	146.52	265.28	333.00	491.72	679.31	895.76	0007	1408-28			2000.	25.80	30.96	39.99	63.21	90-30	170.27	308.30	387.00	571.46	789-47	1041-02	1637.00
1600-		21.09	24-42	32.19	51.06	73.26	134.30	237.53	298.58	439.55	607.16	800-30	•	1259-84			1600.	24.51	28.38	37.41	59.34	85.14	156.08	276.05	347.00	510.83	705.62	930.08	1464-14
4 HILL		18.81	22.20	29.97	46.62	09.99	119.88	205.35	258.62	380.72	526.13	693.74	•			N HILL	1200.	21,93	25,80	34.83	54.18	77.40	139.32	238-64	300.56	445.46	611.45	806.24	1268.06
UP AND DOWN 800.	i i	10.65	19.98	26.64	41.07	58.83	101.01	167.61	210.89	310.79	429.56	566.09	,	7		UP AND DOWN HILL	800	19-35	23-22	30.96	47.73	68.37	117.39	194-79	245.09	361-19	499.22	657-89	1035.86
600	i L	15.54	17.76	24-42	37.74	54.39	89.91	145.41	182.03	268.61	371.84	490-61	77 174	111.44			•009	18.06	20.64	28,38	43.86	63.21	104-49	168.99	211.55	312.17	435.14	570.17	896.54
0.37	, ,	15.54	15.54	21,09	33,30	47.73	76.59	118.77	148.73	219,77	303.02	399.59	70 007	624.36	BLES	0.43	400-	15.48	18.06	24.51	38.70	55.47	89.01	138.02	172,86	255.41	352.16	464.39	731-42
K= 0.		17-71	14.43	19,98	29.97	43.29	68.82	102.12	128.76	189.80	263.06	346.31	C 14 14 14 14 14 14 14 14 14 14 14 14 14	242*00	KRLSP TABLES	K = 0	300.	14.19	16.77	23+22	34.83	50-31	19.98	118.68	149.63	220-58	305.72	402-47	633,38
200*	, (	11.10	13.32	16.65	26.64	38.85	57.72	83.25	105.45	155,39	214.22	283-04	0 1 1 1 1	445.10			200.	12.90	15.48	19.35	30.96	45+15	67,08	96.75	122.55	180.60	248.96	328-94	517.28
R= 300.	) (1) ) (1)	8.8	66*6	13,32	22.20	31.08	04-44	58.83	74.37	109.89	150.95	199.79		314-12		R= 300.	100.	. 10+32	11.61	15.48	25.80	36-12	51-60	68+37	86.43	127-71	175.44	232-20	65-0
505	• · ·	99*9	8,98	11.10	17.76	25.53	33.00	41.07	52-17	77.70	106.56	140.97		222-00			÷0.	7.74	10.32	12.90	20-04	29-67	38.70	47.73	60.63	90*30	123.84	163.83	258.00
1.800	SLOPE	0.25	0.50	1.00	2.C0	3.00	4.00	2.00	9.00	8.00	00-01	12.00		16.00			PERCENT SLOPE	0.25	0.50	1.00	2.00	3.00	4*00	5 <b>~</b> 06	9.00	9-00	10.00	12.00	16.00

2000	29.40 35.28 45.57 72.03 102.90 194.04 351.32 441.00 651.20 899.63 1186.28	2000.	33.00	39.60	80.85	115,50	394,34	495.00	730.94	1009.79	1331,54	2093 • 84
1600.	27.93 32.34 42.63 67.62 97.02 177.86 395.42 582.11 804.08 1059.86 1668.44	1600.	31.35	36.30	75.90	108.90	353.09	443.84	653.39	902-54	1189.64	1872.74
1200•	24.99 29.40 39.69 61.74 88.20 158.76 271.94 342.50 504.20 696.77	N HILL 1200-	28.05	33.00	69.30	00*66	305.25	384.44	565.94	782.09	1031.24	1621.94
UP ANG DGWN HILL 800. 120	22.05 26.46 35.28 54.39 77.91 133.77 221.97 279.29 411.59 568.88 749.69	UP AND DOWN HILL 800. 120	24.75	29.70	61-05	87.45	150*15	313.49	461.99	638.54	841.49	1324.94
•009	20.58 23.52 32.34 49.98 72.03 119.07 192.57 241.07 355.73 492.44 649.73	*009	23.10	26.40	56.10	30.85	133.65	270.59	399•29	552.74	729-29	1146,74
400•	17.64 20.58 27.93 44.10 63.21 101.43 157.29 196.98 291.05 401.30 529.19 833.48	ABLES 0.55	19.80	23.10	49.50	70.95	113.85	221.10	. 326-63	450.44	593.99	935.54
K= 0. 300•	16.17 19.11 26.46 39.69 51.33 91.14 135.24 170.51 251.36 348.36 458.63	KRLSP TABLES K= 0.55 300.	18,15	21.45	44.55	64.35	102.30	191.39	282-14	391.04	514.79	810.14
200.	14.70 17.64 22.05 35.28 35.28 76.44 110.24 139.65 283.70 374.84 589.46	200•	16.50	19.80	39.60	57.75	85.80	156-75	231.00	318.44	420-34	99-199
R= 300. 100.	11.76 13.23 17.64 29.40 41.16 58.80 77.91 98.49 145.52 199.92 264.59	R= 300. 100.	13.20	14.85	33,00	46.20	00-09	110.55	163,35	224.39	297.00	466-94
•05	8.82 11.76 14.70 23.52 33.81 44.10 54.39 69.09 102.00 141.11 186.69	5 5 *	06.0	13.20	16.50	37.35	49.50	77.55	115.50	156,39	209-55	330.00
PERCENT SLOPE	0.25 0.50 1.00 1.00 2.00 2.00 5.00 6.00 12.00 12.00	PCRCENT	SLCPE	73.50	1.00 2.05	3.03	4,00	0.0 0.0	S C C	10.00	12.00	00-91

2000	9.75 11.70 15.11 23.88 34.12 64.35 116.51 146.25 215.96 298.34 393.41 618.63	2000-	11.05 13.26 17.12 27.07 38.67 72.93 132.04 165.75 244.75 338.13
1600.	9.26 10.72 14.13 22.42 32.17 58.98 104.32 131.13 193.04 266.66 351.48	1600.	10.49 12.15 16.02 25.41 36.46 66.85 118.23 148.62 218.78 302.21 398.23
IN HILL 1200.	8.28 9.75 13.16 20.47 29.25 52.65 90.18 113.58 167.21 231.07 304.68	1200.	9.39 11.05 14.91 23.20 33.15 59.67 102.21 128.73 189.50 261.88
UP AND DOWN HILL 800. 120	7.31 8.77 11.70 18.03 25.83 44.36 73.61 92.62 136.50 188.66 248.62 391.46	UP ANG DOWN 800.	8.28 9.94 13.26 20.44 29.28 50.27 83.42 104.97 154.70 213.81
•009	6.82 7.80 10.72 16.57 23.88 39.48 63.86 117.97 163.31 215.47	•009	7.73 8.84 12.15 18.76 27.07 44.75 72.37 90.61 133.70 185.08 244.20
400-	5.85 6.82 9.26 14.62 20.96 33.63 52.16 65.32 133.08 175.50 276.41	0.17	6.63 10.49 16.57 23.75 28.12 59.11 74.03 109.39 150.83
K= 0 300.	5.36 6.33 8.77 13.16 19.01 20.22 44.85 56.55 68.36 115.53 115.53 122.10 172.10 172.10 172.10	K≂ 0.	6.07 7.18 9.94 14.91 21.54 34.25 50.83 64.09 94.47 130.94 172.38
200•	4.87 5.85 7.31 11.70 11.70 25.35 36.56 46.31 66.25 94.08 124.31	200.	5.52 6.63 8.28 13.28 19.33 28.73 41.43 52.48 77.35 140.68
R= 325. 100.	3.90 4.38 5.85 9.75 13.65 19.50 22.66 48.26 66.30 87.75	R= 325. 100.	4.42 6.63 11.05 11.05 15.47 22.10 29.28 37.01 54.69 75.14
50*	2.92 3.90 4.87 7.80 11.21 14.62 18.03 22.91 34.12 46.80 61.91	÷0¢	3.31 4.42 5.52 8.84 12.70 16.57 20.44 25.96 38.67 53.04
PERCENT	0.25 0.50 1.00 2.00 2.00 3.00 4.00 6.00 6.00 10.00 16.00	PERCENT SLOPE	0.25 0.50 1.00 2.00 8.00 6.00 10.00 16.00

2000.	13.00 15.60 20.15 31.85 45.50 85.80 155.35 195.00 287.94 397.79 524.54	2000-	15.60 18.72 24.18 38.22 54.60 102.96 186.42 234.00 345.53 477.35
1600.	12.35 14.30 18.85 29.90 78.65 139.10 174.85 257.39 355.54 468.64	1600.	14.82 17.16 22.62 35.88 51.48 94.38 166.92 209.81 308.87 426.65 562.37
1200•	11.05 13.00 17.55 27.30 39.00 70.20 120.25 151.45 222.95 308.09 406.25 638.94	N HILL 1200.	13.26 15.60 21.06 32.76 46.80 84.24 144.30 181.74 267.53 369.71 487.50
UP AND DOWN HILL 800- 120	9.75 11.70 15.60 24.05 34.45 59.15 98.15 123.00 182.00 251.55 331.49	UP ANC OGWN HILL 800. 120	11.70 14.04 18.72 28.86 41.34 70.98 117.78 148.20 218.39 301.85 397.79
-009	9.10 10.40 14.30 22.10 31.85 52.65 85.15 106.60 157.29 287.29 451.75	<b>*</b> 009	10.92 12.48 17.16 26.52 38.22 63.18 102.18 127.92 188.75 261.29 344.75
6.20	7.80 9.10 12.35 19.50 27.95 44.85 69.55 87.10 128.70 177.44 234.00	ABLES 0.24 400.	9.36 10.92 14.82 23.54 53.85 63.82 83.46 104.52 154.44 212.93 442.25
K≅ 0 300.	7.15 8.45 11.70 17.55 25.35 40.30 59.80 75.40 111.15 154.05 319.14	KRLSP TABLES K= 0.24 300.	8.58 10.14 14.04 21.05 30.42 48.36 71.76 90.48 133.38 184.86 243.36
200-	6.50 7.80 9.75 15.60 22.75 33.80 48.75 61.75 91.00 125.45 165.75	200-	7.80 9.36 11.70 18.72 27.30 40.56 58.50 74.10 109.20 150.54 198.89
R= 325. 100.	5.20 7.85 7.85 13.00 18.20 26.00 34.45 43.55 64.35 88.40	R= 325. 100.	6.24 7.02 9.36 15.60 21.84 31.20 41.34 52.26 77.22 106.08 140.40
÷05	3.90 6.20 10.40 14.95 19.50 24.05 45.50 62.55 130.00	50.	4.68 6.24 7.50 112.48 17.94 23.40 23.86 35.66 54.60 14.88
PERCENT SLOPE	0.25 1.00 2.00 3.00 4.00 5.00 6.00 12.00 16.00	PERCENT SLOPE	0.25 0.50 1.00 2.00 2.00 8.00 10.00 16.00

PERCENT SLOPE	\$0°	R= 325. 100.	200•	K= 0 300.	0.28 400.	•009	UP AND DOWN HILL 800. 120	1 HILL 1200.	1600.	2000-
0.25	5.46	7.28	9.10	10.01	10.92	12.74	13.65	15.47	200	
0.50	7.28	8.19	10.92	11.83	12-74	14.56	16.38	10.00	67 06	18.20
1.00	9.10	10.92	13.65	16.38	17.29	20-02	21.84	07*07	20.02	21 - 84
2.00	14.56	18.20	21.84	24.57	27.30	30.94	73.67	70.00	KO*07	78.21
3.00	20.93	25.48	31,85	35.49	39.13	77	י י י	77.00	41.00	44.09
4.00	27.30	36.40	47.32	56.42	62-79	72 71	10.50	24.00	90.09	63.70
5.00	33.67	48.23	68-25	83.72	72 70	1000	T0*20	87*86	110.11	120.12
9.00	42.77	40.97	57.48	74401	7	170671	19.161	168.35	194.73	217.48
8-00	70 70		0.00	00.00	121.34	149.24	172-89	212.02	244.78	273.00
) C	000	5	121-40	155.60	180-17	220-21	254.79	312.12	360.35	403 12
Э,	01.30	25	175.63	215.67	248.42	304.84	352,16	421 22	70.00	3 F C
12.00	115.57	163.80	232.04	283.91	327.59	402.21	7777	24.0 74	01 1 1 1 1	2000
o	182,00	57.	364.90	446 RD	- 0	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	NO 1	1000	4	134.36
			•	0	17	032-44	730.72	894.52	1032.84	1154.78
				KRLSP TABLES	BLES					
PERCENT SLOPE	\$0°	R= 325. 100.	200.	K= 0 300.	0.32	-009	UP AND DOWN HILL 800. 120	HILL 1200.	1600.	2000*
,										)
0.25	6.24	8.32	10.40	11.44	22.61		1			
0.50	8.32	9.36	17.48	12 62	01-77	14.30	15.60	17.68	19.76	70.80
1.00	10.40	12.48	5 4 5	10.00	14.00	16.64	18.72	20.80	22.88	24.95
2.00	16.64	20.80	***	7.00	9/*67	22.88	24.96	28.08	30.16	37. 62
3.00	23.92	20.00	24.70	28.08	31+20	35,36	38.48	43-6R	70.17	24.04
4-00	31,20	27.52	70°40	40.56	44.72	50.96	55.12	62.69	*****	96.00
5-00	0 0 0 0	00 1	24.08	64.48	71-76	84-24	77 70	7.7.	****	08.2)
200	0	21.66	78.00	95.68	111.28	124 24	+0.+.	114.32	125.84	137.28
	48.88	69.68	98.80	120.64	120 24	77007	40.161	192.40	222.56	248 - 56
	72.80	102,96	145.60	177.83	000	110.36	197.60	242.32	279.75	312.00
<b>.</b>	9.8	141.44	200-22	246 60	20.000	79.167	291.20	356.71	411.83	440 73
12.00	132.08	187.20	265.20	000000000000000000000000000000000000000	16-587	348.40	402-47	492.95	568.87	426 67
v	08-0	294.32	417.02	14.476	3 (4.40	0	530.39	650,00	740482	~ t c c c c c c c
	ı	J 3 1	41.00	510.64	289-67	722.79	835.11	1022,31	1191.00	17*668
							!	1	A 1 0 0 4 4	CJ * KTCT

;	2000°	24.05	28.86	37.27	58.92	84.17	158.73	287.39	360.74	532.70	735.92	970.41	1525.97				2000-	27.95	33.54	43.32	68.43	97.82	184.47	334.00	419.24	619.09	855.26	1127.78	1773.42
	1600.	22.84	26.45	34.87	55.31	79.36	145.50	257.33	323.47	476.18	657.76	867.00	1364,83				1600.	26.55	30.74	40.52	64-28	92.23	169.09	299.06	375.92	553,40	764.43	1007.59	1586-16
HILL	1200-	20-44	24.05	32.46	50.50	72.15	129.86	222-46	280.18	412.45	569.95	751.56	1182,05			N HILL	1200.	23.75	27.95	37.73	58.69	83.85	150.92	258.53	325.61	479.34	662,41	873.43	1373,74
UP AND DOWN HILL	*00°	18-03	21.64	28.86	64.44	63,73	109-42	181.57	228.47	336,69	465,36	613.27	965.60			UP AND DOWN HILL	8008	20-96	25-15	33.54	51.70	74.06	127-17	211.02	265.52	391.29	540.83	712.72	1122-19
	-009	16.83	19.24	26.45	40.88	58.92	97.40	157.52	197,20	291.00	402.83	531.50	835.73				-009	19.56	22.36	30,74	47.51	68.47	113,19	183.07	229,18	338.19	468-16	617,69	971-26
	400*	14.43	16.83	22.84	36.07	51.70	82+97	128.66	161,13	238.09	328.28	432.89	681.81		BLES	0.43	<b>4</b> 00 <b>*</b>	16.77	19.56	26.55	41.92	60.09	96.42	149.53	187-26	276.70	381.51	503.09	792.38
K= 0.37	300.	13.22	15,63	21.64	32.46	46.89	74.55	110.63	139.48	205.62	284.99	375-17	590.42	,	KRLSP TABLES	% ₩	300.	15.37	18.16	25.15	37.73	54-50	86.64	128.57	162.10	238-97	331.20	436.01	686.17
	200-	12.02	14.43	18,03	28.86	42.08	62.53	90.18	114.73	168.35	232.08	336.63	482.20				200-	13.97	16.77	20.96	33.54	48.91	72.67	104.81	132.76	195.64	269.71	356.36	560,39
R= 325.	100.	6-62	10.82	14.43	24.05	33.67	48-10	63.73	80.56	119.04	u	4	340.30			R= 325.	100.	11.18	12.57	16.77	27.95	39.13	55.90	74.06	93.63	138,35	190.05	251.54	395.49
	20.	7.21	6.62	12.02	19.24	27.65	36.07	64.44	56.51	84-17	115.44	152.71	240.50				- 20-	8. 38	11.18	13.97	22.36	32.14	41.92	51.70	65,68	97.82	134,16	177,48	279,50
	PERCENT SLOPE	0.25	0.50	00.	2.00	20-4	7-00	5.00	00-9	00	00-01	, 0	16.00				PERCENT SLOPE	35.0	0.50	1.00	2.00	3,00	4.00	5.00	6-30	8,00	10.00	12.00	

2000•	31.85 38.22 49.36 78.03 111.47 210.20 380.60 477.75 705.47 974.60		2000-	35.75 42.90 55.41 87.58 125.92 235.95 427.21 536.25 791.86 1093.94 1442.51
1600.	30.25 35.03 46.18 73.25 105.10 192.69 340.79 428.38 630.62 871.09 1148.19		1600.	33.96 39.32 51.83 82.22 117.97 216.28 382.52 480.83 707.84 977.76
*N HTLL 1200.	27.07 31.85 42.99 66.88 95.55 171.98 294.61 371.05 546.22 754.84 995.31		N HILL 1200.	30.38 35.75 48.26 75.07 107.25 193.05 330.68 613.11 847.27
UP AND DOWN HILL 800. 120	23.88 23.66 28.26 38.22 58.92 84.40 144.91 240.46 302.57 445.89 616.29 812.17		UP AND DOWN HILL 800-	26.81 32.17 42.90 66.13 94.73 162.66 269.91 339.62 500.49 691.76 911.76
*009	22.29 25.48 35.03 54.14 78.03 128.99 208.61 261.16 385.38 533.48 703.88		+009	25.02 28.60 39.32 60.77 60.77 87.58 144.78 234.16 293.14 432.57 598.81 790.07
0.49	19.11 22.29 30.25 47.77 68.47 109.88 170.39 213.39 315.31 434.75 573.29	BLES	400.	21.45 25.02 33.96 53.62 16.86 191.26 239.52 353.92 643.49
K= (	17.51 20.70 28.66 42.99 62.10 98.73 146.51 184.72 272.31 377.42 496.85	KRLSP TABLES	K= 0 300.	19.66 22.13 48.26 69.11 110.82 164.45 207.45 305.66 423.63 877.66
200-	15.92 19.11 23.88 38.22 36.22 55.73 151.28 151.28 406.08 638.59		200.	17.87 26.81 26.81 42.90 62.95 92.95 134.06 169.81 250.25 344.98 455.81
R= 325. 100.	12.74 14.33 19.11 31.85 44.59 63.70 84.40 106.69 157.65 216.57 286.64		R= 325. 100.	14.30 16.08 21.45 35.75 50.05 71.50 94.73 119.76 176.96 243.10 321.75 505.86
50.	9.55 112.74 15.92 25.48 36.62 47.77 58.92 74.84 111.47 112.88 202.24 318.50		\$0 <b>.</b>	10.72 14.30 17.87 28.60 41.11 53.62 66.13 84.01 125.12 171.60 227.01
PERCENT SLOPE	0.25 0.50 1.00 2.00 3.00 4.00 5.00 10.00 12.00		PERCENT SLOPE	0.25 0.50 1.00 2.00 2.00 6.00 8.00 12.00 16.00

		R= 350.		K S	0.15		UP ANC DOWN HILL	HILL		
PERCENT SLOPE	\$0.	-	200.		<b>-</b> 00+	•009	800-	1200•	1600-	2000-
0.75	3.15	4.20	5.25	5.77	6.30	7,35	7.87	8.92	76.6	10.50
0.50	4.20	4-72	6.30	6.82	7.35	8-40	9-45	10.50	11.55	12.60
00.4	7.75	6-30	7.87	9.45	6.63	11,55	12.60	14.17	15.22	16.27
2-00	8-40	10.50	12-60	14,17	15.75	17.85	19.42	22-05	24.15	25.72
200	12.07	14.70	18-37	20.47	22.57	25.72	27.82	31,50	34-65	36 • 75
00-4	15.75	21.00	27.30	32,55	36.22	42.52	47.77	56.70	63.52	69-30
5.00	19-47	27.82	39-37	48,30	56-17	68,77	79-27	97,12	112.35	125.47
6-06	24.67	35.17	49.87	06-09	70.35	86.10	99.75	122,32	141.22	157.50
8	34. 75	51.07	73.50	89.77	103,95	127.05	147.00	180.07	207.89	232.57
	20.4	77.7	101.32	124.42	143.32	15.87	203_17	248-84	287.17	321-29
0 0	01401	1	122 87	162 70	00.08	232.04	267.74	328.12	378.52	423.67
12-00	10.00		10000	61.0T		10.00	+ 1 1 1 1 1 1	٠	1 1	
16.00	105,00	148.57	210.52	257.77	297-67	364.87	421-57	516.07	595.87	666.22
				KRLSP TABLES	BLES					
		R= 350.		K#	0.17		UP AND DOWN HILL	4 HILL		
PERCENT	50.	100-	200-		400*	-009	800	1200.	1600.	2000.
SLOPE	1									
0.25	3.57	4.76	5.95	6.54	7.14	8-33	8.92	10.11	11.30	11.90
0.50	4.75	5.35	7-14	7.73	8.33	9.52	10.71	11.90	13.09	14.78
Ç,	40.0	7.14	8.92	10.71	11.30	13.09	14.28	16.06	17.25	18.44
2-00	9.52	11.90	14.28	16.06	17.85	20-23	22.01	24.99	27.37	29-15
3.00	13.68	16.66	20.82	23,20	25.58	29-15	31.53	35.70	39.27	41.65
6-00	17.85	23.80	30-94	36.89	41.05	48.19	54.14	64.26	71.99	78.54
5.00	22.01	31.53	44-62	54.74	63.66	77.94	89.84	110.07	127.33	142.20
00.49	27.96	39-86	56.52	69.02	79.73	97.58	113.05	138.63	160.05	178.50
8.00	41.55	58.90	83+30	101.74	117.81	143.98	166.60	204.08	235.61	263,58
10.00	57.12	80.92	114.83	141-01	162,43	199-32	230.26	282,02	325.46	364-13
12.00	75.56	107.10	151.72	185.64	214.20	262.98	303.44	371.87	458.99	480-16
16.00	119,00	168.38	238.59	292.14	337-36	413.52	477.78	584.88	675.32	155.05

2000-	14.00 16.80 21.70 34.30 49.00 92.40 167.30 210.00 310.09 428.39 564.89		2000*		٥	10.00	20.16	26.04	41-16	58.80	110.88	200.76	752.00	372 11	514.07	677.87	1065.95
1600.	13.30 15.40 20.30 32.20 46.20 84.70 149.80 188.29 277.19 382.89 504.69		1600.		15.96	07.0	70.40	24.30	38.64	22.44	101.64	179.76	225.95	332,63	459.47	605,63	953.39
N HILL 1200.	11.90 14.00 18.90 29.40 42.00 75.60 129.50 163.10 240.10 331.79 437.50		HILL 1200.						22 - 58		90.72	55.40	95.72	88-11	98.15		825.71
UP AND DOWN HILL 800. 120	10.50 12.60 16.80 25.90 37.10 63.70 105.70 135.00 196.00 270.90		UP AND DOWN 860.		12.60	15-12	20-16	31.0	44.52	17 71	126.04	120.84	159.60	235-19	525-07	428-39	674.51
<b>•</b> 009	9.80 11.20 15.40 23.80 34.30 56.70 91.70 114.80 169.39 234.50 309.39		<b>.</b> 009	;	11.76	13-44	18-48	28.56	41-16	68.04	110-04	127 76	10.00	2002	244	77.77	303-13
0.20	8.40 9.80 13.30 21.00 30.10 48.30 74.90 93.80 138.60 191.09 252.00	BLES	0.24	0	200	11.66	15.96	25-20	36.12	57.96	89.88	112.56	166-32	220.22	302.39	476.27	•
K= (	7.70 9.10 12.60 18.90 27.30 43.40 64.40 d1.20 119.70 165.90 218.40	KRLSP TABLES	K= 0 300.	40.0	10.07	7	27 - 62	20.77	32.76	80.25	77.28	44.26	143.64	199,08	62.	77	
200•	7.00 8.40 10.50 16.80 24.50 36.40 52.50 66.50 98.00 135.10 178.50		200-	8.40	10.08	12.60	20-16	200	07.67	00.00	03.00	79.80	117-60	162.11	214.19	336.83	
R= 350. 100.	5.60 6.30 8.40 14.00 19.63 28.00 37.10 46.90 69.30 95.20 126.00		R= 350. 100.	6.72	7.56	10-08	16.80	23.52	33.60	C 2 77	70°	22.00	4	14-2	151-20	) (	
50.	4.20 5.60 7.00 11.20 16.10 25.90 32.90 49.00 67.20 88.90		50.	5.04	6-72	8-40	13.44	19-32	25-20	31.08	87.68	0 0		\$0. 90. 90.	10000000000000000000000000000000000000		
PERCENT SLOPE	0.25 0.50 1.00 2.00 3.00 4.00 5.00 6.00 12.00 16.00		PERCENT SLOPE	0-2>	000	000	2.00	3.00	4.00	2.00	6.00	8.00	10-00	12.00	36.00	) )	

KRLSP TABLES

	2000.	19.60	23.52	30.38	48.02	68.60	129.36	234-22	294.00	434-13	599.75	790.85	1243.61				2000	22.40	26.88	34.72	54.88	78.40	147.84	267.67	336.00	496-15	685.43	903-83	1421.27
	1600.	18-62	21.56	28.42	45.08	64.68	118.58	269.72	263.61	388.07	536.05	706.57	1112.29				1600.	21.28	54.64	32.48	51.52	73-92	135.52	239-68	301.27	443.51	612.63	807.51	1271-19
HILL	1200.	16.66	09.61	26.46	41.16	58.80	105.84	181.30	228.33	336,13	464.51	612.49	963.33			HILL	1200.	19.04	22.40	30,24	41.04	67.20	120.96	207.20	260.96	384.15	530.88	700.00	1100.95
UP AND DOWN HILL	800°	14.70	17.64	23.52	36.26	51.94	89.18	147.98	186.20	274.39	379.25	466,79	786.93			UP AND DOWN HILL	800	16.80	20.16	26.38	41.44	26*36	101,92	169.12	212.80	313,59	433.44	571.19	899.35
	*009	13.72	15.68	21.56	33,32	48.02	79.38	128.38	160.72	237-15	328-29	433-15	681.09			•	•009	15.68	17.92	24.64	38.08	54.88	90.72	146.72	183.68	271.03	375.20	495.03	778.39
0.28	400*	11.76	13.72	18.62	29.40	45-14	67.62	104.86	131.32	194.03	267.53	352.79	555.65		BLES	0.32	400*	13.44	15.68	21.28	33.60	48.16	77.28	119.84	150.08	221.76	305.75	403.20	635.03
	300-	10.78	12.74	17.64	26-46	38.22	60.76	90-16	113.68	167.57	232-26	305.75	481.17		KRLSP TABLES		300.	12.32	14.56	20.16	30.24	43-68	69.44	103.04	129.92	191.52	265.44	349.44	549.91
	200-	9.80	11.76	14.70	23-52	34.30	50.96	73.50	93.10	137.20	189.13	249.89	392-97				200-	11.20	13.44	16.80	26.88	39.20	58.24	84.00	106.40	156.80	216.16	285.59	449.11
R= 350.	100.	7.84	8.82	11.76	19.60	27.44	39.20	51.94	65.66	97.02	133.27	176,40	277.33			R= 350.	100-	96*8	10.08	13,44	22.40	31,36	44.80	59.36	75.04	110.88	152,32	201,60	316.96
	\$0°	5. 88	7.34	9-80	15.68	22.54	29-40	36.26	46.06	68.60	94.08	124-46	196-00				50.	6.72	8*96	11.20	17.92	25.76	33.60	41.44	52.64	78.40	107.52	142.24	224.00
	PERCENT SLOPE	0.25	0.50	1.00	2.00	3.00	4.00	5.00	9.00	8.00	10.00	12-00	16.00	•			PERCENT SLOPE	0.25	0.50	1.00	2,00	3.00	4.00	۰۰۰۰	6.00	3.00	10.00	12.00	16.00

2000-	25.90	31.08	40-14	63.45	90.65	170.94	01.00%	00.000	61.000	010-06	66.261	1045-06	1643.35			2000-		30.10	36.12	46.64	73 . 74	105.35	198-66	350 60	60.00	451.49	666.71	921.05	1214.53	1909 92
1600.	24.60	28.49	37.55	59.57	85.47	156.69	277.12	24.845	10.010	10.277	95.801		1469.82			1600.		28.59	33.11	43.64	69.23	99,33	187.10	322-06	200	オロ・ナンナ	595.97	823.23	1085.10	1708-17
AN HILL 1200.	22-01	25.90	34.96	54.39	77.70	139.86	739.57	301.73	466.10	0 0 0	70.610	20.400	1272.98		N HILL	1200-	;	25.58	30-10	40-63	63.21	90.30	162.54	278.42	77 032	00-000	516.21	713.36	940.62	1479.41
UP AND DOWN HILL 800•	19-42	23.31	31.08	47.91	68.63	117.84	195,54	246-04	342,50		707-107	****	1039.88		UP AND DOW	800- 1200-	4	14.22	27.09	36.12	55.68	79.76	136.95	227.25	285.94	1000	461.34	582,43	767.54	1208.51
*009	18*13	20.12	28.49	44.03	63.45	104.89	169.64	212.37	313,38	00 707	מני כיר א	000000	20.006			<b>*</b> 009	7	10.13	24.08	33.11	51.17	73.74	121-90	197-15	246.81	40. 736	02*100	504-17	665.20	1045.97
0.37	15.54	18.13	24-60	38.85	55.68	89.35	138.56	173.52	256.40	252 52	666	, , , ,	134.26	BLES	0.43	400*	3.	0 0 0	70-17	28-59	45.15	64-71	103.84	161.03	201.66	30 100	06.117	410.80	-	853.33
300°	14.24	16.83	23.31	34.96	50.50	80.29	119.14	150.22	221.44	306.91	404-03	70 367	022-84	KRLSP TABLES		300•	14 71		14,00	60*/2	40*63	58.69	43.31	138.46	174.57	257.25	25.4.0	00.000	ָ ס	738.95
200-	12.95	15.54	19-42	31.08	45+32	67-34	97.12	123.02	181.29	249-03	330.22	010	62.616			200-	15.04	4	1010	16-22	36-12	74.67	97.87	112.8/	145.97	210.69	290 44	1000	11.000	603.50
R= 350. 100.	10.36	11.65	15.54	25.90	36.26	51.80	68.63	86.76	128.20	176.11	233_10	244 40	5		R= 350.	100	12.04	75 61	100	0 0 0 0 0	07.00	+T+7+	00.00	0.00	100.83	148.99	204.67	370 00		16-674
-05	7.77	10.36	12,35	20.72	29.78	38+85	16-17	98*09	90.06	124.32	164 46	250 00	•		í	*0.5	9,03	12.04	40.4	000	20-47	70. 27	07 33	00.00	5) "0"	105.35	144.48	101		201
PERCENT SLOPE	0.25	0.00 0.00	1.00	2.00	3•00	4.00	2*00	00-9	8.00	10-00	12.00	16.00			i i	SLOPE	D.25	0.50	1.00		200	3	00	200	)	8*00	10.00	12,00	14.00	00 * 0

2000.	34.30 41.16 53.16 84.03 120.05 226.38 409.88 514.49 759.74 1049.57 1384.00	2000*	38.50	59.67	94.32	134.75	254.10	460-07	577.49	852.17	1178.09	1553.47	2442.82
1600.	32.58 37.73 49.73 78.89 113.19 207.51 367.00 461.33 679.13 938.10 1236.51	1600.	36.57	55.82	88.55	127.05	232.92	411-94	517.82	762-29	1052.97	1387,92	2184.87
N HILL 1200.	29.15 34.30 72.03 102.90 185.22 317.27 399.59 588.24 812.90 1071.87	1200.	32.72	51.97	80.85	115.50	207.89	356.12	448.52	660.27	912.44	1203.12	1892.27
UP AND DOWN HILL 800. 120	25.72 30.87 41.16 63.45 90.89 156.06 258.96 325.84 480.19 663.70 874.64	UP AND DOWN HILL 800. 120	34.65	46.20	71-22	102.02	175-17	290.67	365.74	538.99	744.97	981.74	1545.77
-009	24.01 27.44 37.73 58.31 84.03 138.91 224.66 281.25 415.02 574.52 758.02	•009	26.95 30.80	42.35	65.45	94,32	155.92	252.17	315.69	465-84	644.87	850.84	1337,87
400*	20.58 22.58 32.58 51.45 73.74 118.33 183.50 229.80 339.56 468.19 617.39 972.40	0.55	23.10	36.57	57.75	82.77	132-82	205-97	257.94	381-14	525.52	692-99	1091.47
K= 0 300.	18.86 22.29 30.87 46.39 106.33 117.77 198.94 293.26 406.45 406.45 406.45 842.06 97		25.02	34.65	51.97	75.07	119.35	177-10	223.29	329.17	456.22	690,59	945.17
200-	17.15 20.58 25.72 41.16 60.016 89.18 162.92 162.92 240.09 437.32 687.71	200.	19.25 23.10	28-87	46.20	67.37	100-10	144-37	182.87	569.49	371.52	490.87	771.92
R= 350. 100.	13.72 15.43 20.58 34.30 48.02 68.60 90.89 114.90 114.90 233.23 308.69 485.34	R= 350.	17.32	23-10	38.50	53.90	77.00	102.02	128.97	190.57	261.79	346.50	544.77
50.	10.29 13.72 17.44 27.44 39.44 51.45 63.45 80.60 120.05 164.64 217.80 343.00	50.	15.40	19.25	30.80	44.27	51.75	71-22	25.06	134.75	184.79	244.47	385.00
PERCENT SLOPE	0.25 0.50 1.00 2.00 3.00 3.00 4.00 6.00 12.00 16.00	PERCENT SLOPE	0.50	1.00	2.00	3-00	00.4	5.00	9.00	3.00	10.00	12.00	16.00